TOSHIBA Bi-CMOS Integrated Circuit Silicon Monolithic

# **TB6585FG, TB6585FTG**

3-Phase Sine-Wave PWM Driver for BLDC Motors

#### **Features**

- Sine-wave PWM drive
- Triangular-wave generator
- Hall amplifier
- Lead angle control
- Current limit control input  $(V_{RS} = 0.5 V (typ.))$
- Rotation pulse output (3 pulse/electrical degree 360°)
- Operating supply voltage range:  $VM = 4.5$  to  $42$  V
- Reference supply output:  $V_{refout} = 4.4 V (typ.), 20 mA (max)$
- Output current:  $I_{OUT} = 1.8 A (max), 1.2 A (typ.)$  (FG type)

 $IOUT = 1.0 A (max), 0.8 A (typ.) (FTG type)$ 

• Output On-resistance:  $R_{on}$  (P-channel and N-channel sum) =  $0.7 \Omega$  (typ.)



Weight: HSOP36-P-450-0.65: 0.79 g (typ.) QFN48-P-0707-0.50: 0.137 g (typ.)

#### **Pin Assignment**

#### **TB6585FG**



Note: Pins 1 and 36 and pins 18 and 19 are respectively connected together on the frame inside the IC. The NC pin can be used as a jumper. The fin and the package bottom are electrically connected. To stabilize the chip, the Fin pins should be connected to S-GND and P-GND at a location as close to the TB6585FG as possible.

**TB6585FTG**



### **Pin Description**



## **I/O Equivalent Circuits**

Some parts are omitted from the equivalent circuit diagrams or simplified for the sake of simplicity.



## TB6585FG/FTG



## TB6585FG/FTG



## **Absolute Maximum Ratings (Ta = 25°C)**



Note 1: Output current may be limited by the ambient temperature or a heatsink. The maximum junction temperature should not exceed  $T_{jmax}$  = 150°C.

Note 2: Measured for the IC only.  $(T_a = 25^{\circ}C)$ 

Note 3: Measured on a board. (100 mm  $\times$  200 mm  $\times$  1.6 mm, Cu: 50%)

### **Operating Ranges (Ta = 25°C)**



## **Package Power Dissipation**

#### **TB6585FG**



- (1) Rth (j-a): 96°C/W
- (2) Measured on a board (114 mm  $\times$  75 mm  $\times$  1.6 mm, Cu: 20%) R<sub>th (j-a)</sub> = 65°C/W
- (3) Measured on a board (140 mm  $\times$  70 mm  $\times$  1.6 mm, Cu: 50%) R<sub>th</sub>  $_{(j-a)} = 39^{\circ}$ C/W



#### **TB6585FTG**

Measured on a board (140 mm  $\times$  70 mm  $\times$  1.6 mm, Cu: 50%) Rth (j-a) = 38°C/W

## **Electrical Characteristics (Ta = 25°C, VM = 24 V)**





Note: Product testing before shipment is not performed.

### **Functional Description**

#### **1. Basic Operation**

At startup, the motor is driven by a square-wave commutation signal that is generated based on the position detection signal. When the position detection signal exceeds the rotational frequency of  $f = 2.5$  Hz, the rotor position is determined by the position detection signal and the modulated wave signal is generated. Then, the sine-wave PWM signal is generated by comparing the modulated wave signal with the triangular wave signal to start a motor in PWM drive mode.

Startup to 2.5 Hz: Square-wave drive (120° commutation)  $f = f$ osc/(2<sup>13</sup> × 41 × 6) 2.5 Hz or higher: Sine-wave PWM drive (180° commutation)  $f \approx 2.5$  Hz when  $f_{osc} = 5$  MHz

#### **2.** Speed Control Input (V<sub>SP</sub>)

- (1) Speed control input:  $0 V < V_{SP} \le 0.5 V$
- The motor-driving output is turned off. (Motor is stopped.)
- (2) Speed control input:  $V_{\rm SP} > 0.5$  V When  $f_{\text{osc}} = 5 \text{ MHz}$ , the motor is driven by a square wave until f reaches 2.5 Hz. Then, the motor-driving signal is switched to a sine-wave signal.



Note: An amplitude of the modulated waveform becomes maximum when  $V_{SP} = V_{refout}$ . The PWM duty cycle that is obtained with the  $V_{SP}$  voltage of  $V_{refout}$  is defined as 100%.

#### **3. Carrier Frequency Setting**

The frequency of the triangular wave (carrier frequency) required for the PWM signal generation is fixed at the following value:

fc = fosc/252 (Hz), where fosc = Reference clock frequency (RC oscillator frequency)

Example: When  $f_{\text{osc}} = 5 \text{ MHz}$ ,  $f_c = 19.8 \text{ kHz}$ 

#### **4. Lead Angle Correction**

The lead angle of the motor driving signal generated in accordance with the induced voltage (Hall signal) is corrected by an angle between 0 and 29°.

The lead angle control can be achieved by directly applying a voltage to the LA pin, or by using the motor current.

### **<Simplified Diagram of the LA Pin>**



#### **<Typical Characteristics of the LA versus Lead Angle>**







#### **<Simplified Diagram of the Automatic-Lead-Angle Correction Circuitry>**



\*: Gain =  $(R_1 + R_2) / R_1$ ,  $R_3 = 100$  kΩ,  $C_1 = 0.1$  µF



#### **5. Position Detection (Hall effect input)**

The in-phase input voltage range, VCMRH, is from 1.5 to 3.5 V. The input hysteresis, VH, is 8 mV (typ.).



 $*$ : The Hall amplifier can operate when  $V_S$  is at least 50mVpp. However, to stabilize the time interval between zero-cross points of each phase signal, that is, the 60-electrical-degree interval, the amplitude should be as high as possible. (VS is recommended to be 200 mVpp or higher.)

#### **6. Rotation Pulse Output (FG output)**

This pin generates a rotation pulse (3 pulses/electrical degree). Example: With an eight-pole motor, 12 pulses are generated per revolution. (12 ppr)

#### **7. Reverse Rotation Detection**

The direction of the motor rotation is detected. The drive mode is then selected between 120° commutation and 180° commutation modes.

The detection is performed at every electrical degree of 360°.



Note: When the Hall signal frequency is below 2.5 Hz, the TB6585FG/FTG is put in 120° commutation mode even when 180° commutation mode is selected.

#### **8. Various Protections**

(1) Overcurrent Protection (RS pin)

When a DC link current exceeds the internal reference voltage, output transistors are turned off. The TB6585FG/FTG exits overcurrent protection mode every carrier cycle. Reference voltage = 0.5 V (typ.)

(2) External RESET (RESET pin)

Output transistors are turned off when RESET is High; they are turned on again when RESET is Low or Open.

The RESET pin can be used to turn off output if any abnormality is detected externally.

- (3) Internal Protections
	- Position Detection Fault Protection When the position detection signals are all set to High or Low, output transistors are turned off. Otherwise, the motor is restarted every carrier cycle.
	- Anti-lock capability

When the operation mode is not properly switched as configured from 120° commutation mode of startup operation to 180° commutation mode, the motor is deemed to be locked and output transistors are turned off. The restart operation can be selected from either the automatic restart or the power cycling.



 $\leq$ Setting the Time of Motor-Lock Detection and the Time While the Motor is Stationary The time required for the motor-lock detection and the time while the motor driving signal is inactive can be adjusted by the external capacitor  $C_1$ . (These periods are set to be the same.)

Time setting 
$$
T = \frac{C_1 \times V_{th}}{I} \times 1024(s) \qquad I = 0.72 \text{ }\mu\text{A}, \text{ } V_{th} = 2 \text{ V}
$$

Example: When  $C_1 = 180$  pF,  $T \approx 500$  ms (typ.).

 $\triangle$ Automatic Restart (ML = High)

When the Hall signal frequency is kept below 2.5 Hz for at least 500 ms (typ.), the TB6585FG/FTG becomes active and inactive periodically every 500 ms (typ.). The protection is disabled when the Hall signal frequency reaches 2.5 Hz and the operation mode is switched to 180° commutation mode.

 $\langle$ Restart with Power Cycling (ML = Open or Low)

When the Hall signal frequency is kept below 2.5 Hz for at least 500 ms (typ.), output transistors are disabled. The TB6585FG/FTG can be restarted by turning off and back on the VM power supply, which must be kept below 3.5 V (typ.). The TB6585FG/FTG can also be restarted by turning off and back on VSP, which must be kept below  $0.5$  V (typ.).

• Undervoltage Protection (VM Power Supply Monitoring) When the VM power supply is turned on or off, commutation signal outputs are disabled while VM is outside the operating voltage range.



## **Operation Flow**



#### <**Sine-Wave PWM Signal Generation**>

The modulated waveform is generated using the Hall signals. The sine-wave PWM signal is then generated by comparing the modulated waveform with the triangular wave.

The time between the rising edges (falling edges) and the immediately-following falling edges (rising edges) of any of the three Hall signals (interval of 60 electrical degrees) are calculated by the counter. This period is used for data generation of the next 60-electrical-degree interval.

The modulated waveform of 60-electrical-degree interval consists of 32 data items. The time period for a single data item is 1/32 of the previous 60-electrical-degree interval. The modulated waveform advances by this period. (Operating waveforms when CW/CCW = Low)



As illustrated above, the modulated waveform ) (1)'advances by 1/32 of the period between the rising edge ( $\frown$ ) of HU and the falling edge ( $\grown$ ) of HW. Likewise, the modulated waveform (2)' advances by 1/32 of the period between the falling edge  $(\dagger)$  of HW and the rising edge  $(\dagger)$  of HV.

If the next edge does not occur even after completing the generation of 32 data, data for the next 60-electrical-degree interval are generated based on the same time period until the next edge occurs.



Also, the phase alignment with the modulated waveform is performed at every zero-cross point. The modulated waveform is reset by being synchronized with the rising and falling edges of the position detection signal at every 60 electrical degrees. Therefore, the modulated waveform becomes discontinuous at every reset if there occurs a zero-cross point error of the Hall signal, or when motor is being accelerated or decelerated.

Also, the phase alignment with the modulated waveform is performed at every zero-cross point.

The modulated waveform is reset by being synchronized with the rising and falling edges of the position detection signal (Hall amplifier output) at every 60 electrical degrees.

Therefore, if the next zero-cross point occurs before completing the generation of 32 data for 60-electrical-degree interval due to the zero-cross point error of the position detection signal, the current data is reset and the data generation for the next 60-electrical-degree interval is then started. In such cases, the modulated waveform is discontinuous at every reset.



#### **<Output Waveform of the Sine-Wave PWM Drive>**



#### **<Output Waveform of the Square-Wave Drive>**



Note: The above U-phase waveform shows the behavior of the U-phase output signal when a resistor is connected between the U and VM pins and also between the U pin and ground to obtain  $\frac{VW}{L}$ . Likewise, resistors are connected to the V and W pins.  $\frac{V}{V}$  indicates the high-impedance state.  $\frac{2}{V}$ VM  $\overline{2}$ VM

### **Timing Chart of the Clockwise Rotation (CW/CCW = Low, LA = GND)**



#### \*: The lead-angle correction is performed in accordance with the LA input when the Hall signal frequency is 2.5 Hz or higher.

### **Timing Chart of the Clockwise Rotation (CW/CCW = Low, LA = GND)**



\*: If the Hall signal for counterclockwise rotation is applied when CW/CCW = Low, the motor is driven by the 120 $^{\circ}$ commutation signal with a lead angle of 0°. (Reverse rotation by the wind)

### **Timing Chart of the Counterclockwise Rotation (CW/CCW = High, LA = GND)**



\*: The lead-angle correction is performed in accordance with the LA input when the Hall signal frequency is 2.5 Hz or higher.

### **Timing Chart of the Counterclockwise Rotation (CW/CCW = High, LA = GND)**



\*: If the Hall signal for clockwise rotation is applied when CW/CCW = High, the motor is driven by the 120 $^{\circ}$ commutation signal with a lead angle of 0°. (Reverse rotation by the wind)

## **Block Diagram**

**TB6585FG**



## TB6585FG/FTG

### **TB6585FTG**

TOSHIBA



Note: TB6585FG/FTG

Note 1: An oscillation prevention capacitor should be connected to the  $V_{refout}$  pin at a location as close to the TB6585FG/FTG as possible.

If the package's thermal performance is not enough for the application, a load must not be connected to the Vrefout output; instead, a voltage of 4.4 V must be applied externally to it.

- Note 2: An oscillation prevention capacitor should be connected to the VM pin at a location as close to the TB6585FG/FTG as possible.
- Note 3: If there is a significant noise, an RC filter (low-pass filter) should be connected.
- Note 4: A large current or voltage might be abruptly applied to the IC and peripherals in case of a short-circuit across outputs, a short-circuit to power supply or a short-circuit to ground. This possibility should be fully considered in the design of the output, VM, IR and ground lines. Also, care should be taken not to install the IC in the wrong orientation. Otherwise, IC may be broken.
- Note 5: The constants of loads that are connected externally to the IC shown in the above diagram are used as initial values to determine whether the application operates properly. The capacitor values that are connected to VM, V<sub>refout</sub> and between positive and negative inputs of Hall elements must be determined experimentally.

### **Package Dimensions**

**TB6585FG**

HSOP36-P-450-0.65

Unit: mm



Weight: 0.79 g (typ.)

### TB6585FG/FTG

#### **TB6585FTG**

**TOSHIBA** 

QFN48-P-0707-0.50

"Unit : mm"



Weight: 0.137 g (typ.)

#### **Notes on Contents**

#### **1. Block Diagrams**

Some of the functional blocks, circuits, or constants in the block diagram may be omitted or simplified for explanatory purposes.

#### **2. Equivalent Circuits**

The equivalent circuit diagrams may be simplified or some parts of them may be omitted for explanatory purposes.

#### **3. Timing Charts**

Timing charts may be simplified for explanatory purposes.

#### **4. Application Circuits**

The application circuits shown in this document are provided for reference purposes only. Thorough evaluation is required, especially at the mass production design stage. Toshiba does not grant any license to any industrial property rights by providing these examples of application circuits.

#### **5. Test Circuits**

Components in the test circuits are used only to obtain and confirm the device characteristics. These components and circuits are not guaranteed to prevent malfunction or failure from occurring in the application equipment.

#### **IC Usage Considerations**

#### **Notes on handling of ICs**

- (1) The absolute maximum ratings of a semiconductor device are a set of ratings that must not be exceeded, even for a moment. Do not exceed any of these ratings. Exceeding the rating(s) may cause the device breakdown, damage or deterioration, and may result injury by explosion or combustion.
- (2) Use an appropriate power supply fuse to ensure that a large current does not continuously flow in case of over current and/or IC failure. The IC will fully break down when used under conditions that exceed its absolute maximum ratings, when the wiring is routed improperly or when an abnormal pulse noise occurs from the wiring or load, causing a large current to continuously flow and the breakdown can lead smoke or ignition. To minimize the effects of the flow of a large current in case of breakdown, appropriate settings, such as fuse capacity, fusing time and insertion circuit location, are required.
- (3) If your design includes an inductive load such as a motor coil, incorporate a protection circuit into the design to prevent device malfunction or breakdown caused by the current resulting from the inrush current at power ON or the negative current resulting from the back electromotive force at power OFF. IC breakdown may cause injury, smoke or ignition. Use a stable power supply with ICs with built-in protection functions. If the power supply is unstable, the protection function may not operate, causing IC breakdown. IC breakdown may cause injury, smoke or ignition.
- (4) Do not insert devices in the wrong orientation or incorrectly. Make sure that the positive and negative terminals of power supplies are connected properly. Otherwise, the current or power consumption may exceed the absolute maximum rating, and exceeding the rating(s) may cause the device breakdown, damage or deterioration, and may result injury by explosion or combustion.

In addition, do not use any device that is applied the current with inserting in the wrong orientation or incorrectly even just one time.

### **Points to Remember on Handling of ICs**

(1) Over current protection circuit

Over current protection circuits (referred to as current limiter circuits) do not necessarily protect ICs under all circumstances. If the Over current protection circuits operate against the over current, clear the over current status immediately.

Depending on the method of use and usage conditions, such as exceeding absolute maximum ratings can cause the over current protection circuit to not operate properly or IC breakdown before operation. In addition, depending on the method of use and usage conditions, if over current continues to flow for a long time after operation, the IC may generate heat resulting in breakdown.

(2) Thermal shutdown circuit

Thermal shutdown circuits do not necessarily protect ICs under all circumstances. If the thermal shutdown circuits operate against the over temperature, clear the heat generation status immediately. Depending on the method of use and usage conditions, such as exceeding absolute maximum ratings can cause the thermal shutdown circuit to not operate properly or IC breakdown before operation.

(3) Heat radiation design

In using an IC with large current flow such as power amp, regulator or driver, please design the device so that heat is appropriately radiated, not to exceed the specified junction temperature (TJ) at any time and condition. These ICs generate heat even during normal use. An inadequate IC heat radiation design can lead to decrease in IC life, deterioration of IC characteristics or IC breakdown. In addition, please design the device taking into considerate the effect of IC heat radiation with peripheral components.

(4) Back-EMF

When a motor rotates in the reverse direction, stops or slows down abruptly, a current flow back to the motor's power supply due to the effect of back-EMF. If the current sink capability of the power supply is small, the device's motor power supply and output pins might be exposed to conditions beyond absolute maximum ratings. To avoid this problem, take the effect of back-EMF into consideration in system design.

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