## PWM/VFM Step-down DCIDC Controller

NO.EA-097-181004

## OUTLINE

The R1225N is a CMOS-based PWM step-down DC/DC converter controller with low supply current. It consists of an oscillator, a PWM control circuit, a reference voltage unit, an error amplifier, a soft-start circuit, a latchtype protection circuit, a PWM/VFM alternative circuit, a chip enable circuit, a phase compensation circuit, and an input voltage detect circuit. Further, protection circuit delay time adjuster circuit, and resistors for voltage detection are included. A low ripple, high efficiency step-down DC/DC converter can be easily composed of this IC with some external components, or a power-transistor, an inductor, a diode and capacitors. With a PWM/VFM alternative circuit, when the load current is small, the operation is automatically switching into the VFM oscillator from PWM oscillator, therefore the efficiency at small load current is improved. The R1225NxxxC/D/K types, which are without a PWM/VFM alternative circuit, are also available. If the term of maximum duty cycle keeps on a certain time, the embedded protection circuit works. It is latchtype protection circuit, and it works to latch an external Power MOSFET with keeping it off. To release the condition of protection, after disable this IC with a chip enable circuit, enable it again, or restart this IC with power-on. Delay Time for protection circuit is adjustable with an external capacitor. With a built-in UVLO function, when the input voltage is UVLO threshold or less, this IC keeps standby state, and saves its consumption current and avoids miss-operation. Further, if the set output voltage is equal or more than 2.1 V , with a built-in start-up function, at the power-on moment until the input voltage becomes more than the set output voltage, $\mathrm{DC} / \mathrm{DC}$ operation is halted and avoids miss-operation.

## FEATURES

- Wide Range of Input Voltage 2.3 V to 18.5 V
- Built-in Soft-start and Latch-type Protection
- Three Options of Oscillator Frequency............................................ 180 kHz, 300 kHz, 500 kHz
- High Efficiency ................................................................................. Typ. 90\%
- Output Voltage 1.2 V to $6.0 \mathrm{~V}, 0.1 \mathrm{~V}$ step
- Standby Current............................................................................ Typ. $0.0 \mu \mathrm{~A}$
- High Accuracy Output Voltage........................................................ $\pm 2.0 \%$
- Low Temperature-Drift Coefficient of Output Voltage ...................... Typ. $\pm 100 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$


## APPLICATIONS

- Hand-held Communication Equipment, Cameras, VCRs, Camcorders
- Battery-powered Equipment
- Household Electrical Appliances


## BLOCK DIAGRAM



R1225N Block Diagram

## SELECTION GUIDE

The output voltage, the oscillator frequency and the PWM/VFM alternative circuit are user-selectable options.

## Selection Guide

| Product Name | Package | Quantity per Reel | Pb Free | Halogen Free |
| :---: | :---: | :---: | :---: | :---: |
| R1225Nxx2*-TR-FE | SOT-23-6W | $3,000 \mathrm{pcs}$ | Yes | Yes |

$x x$ : The output voltage can be designed in the range from $1.2 \mathrm{~V}(12)$ to $6.0 \mathrm{~V}(60)$ in 0.1 V steps.
*: The oscillator frequency and the modulation method are options as follows.

| $*$ | Oscillator <br> Frequency | PWM/VFM Alternative <br> Circuit |
| :---: | :---: | :---: |
| A | 300 kHz | Yes |
| B | 500 kHz | Yes |
| C | 300 kHz | No |
| D | 500 kHz | No |
| J | 180 kHz | Yes |
| K | 180 kHz | No |

## PIN DESCRIPTIONS



R1225N (SOT-23-6W) Pin Configuration

## Pin Description

| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | EXT | External Transistor Drive Pin, CMOS Output Type |
| 2 | VIN | Power Supply Pin |
| 3 | DLY | Pin for Setting External Capacitor for Protection Circuit Delay Time |
| 4 | CE | Chip Enable Pin, Active-high |
| 5 | GND | Ground Pin |
| 6 | VOUT | Pin for Monitoring Output Voltage |

## ABSOLUTE MAXIMUM RATINGS



## ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause the permanent damages and may degrade the lifetime and safety for both device and system using the device in the field. The functional operation at or over these absolute maximum ratings is not assured.

## RECOMMENDED OPERATING CONDITIONS

Recommended Operating Conditions

| Symbol | Item | Rating | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | Input Voltage | 2.3 to 18.5 | V |
| Ta | Operating Temperature Range | -40 to 85 | ${ }^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if when they are used over such conditions by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.

## ELECTRICAL CHARACTERISTICS

| $\left(\mathrm{Ta}=25^{\circ} \mathrm{C}\right)$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Item | Conditions | Min. | Typ. | Max. | Unit |
| Vout | Step-down Output Voltage | $\begin{aligned} & \mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=\mathrm{V}_{\text {SET }}+1.5 \mathrm{~V} \text {, lout }=-100 \mathrm{~mA} \\ & \text { When } \mathrm{V}_{\text {SET }} \leq 1.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=3.0 \mathrm{~V} \end{aligned}$ | $\begin{gathered} \hline \mathrm{V}_{\text {SET }} \\ \times 0.98 \\ \hline \end{gathered}$ | Vset | $\begin{array}{\|c\|} \hline V_{\text {SET }} \\ \times 1.02 \\ \hline \end{array}$ | V |
| $\Delta$ Vout/ $\Delta \mathrm{Ta}$ | Step-down Output Voltage Temperature Coefficient | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 85^{\circ} \mathrm{C}$ |  | $\pm 100$ |  | $\begin{gathered} \mathrm{ppm} / \\ { }^{\circ} \mathrm{C} \end{gathered}$ |
| fosc | Oscillator Frequency | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\mathrm{CE}}=\mathrm{V}_{\text {SET }}+1.5 \mathrm{~V} \text {, IOUT }=-100 \mathrm{~mA}$ <br> When $\mathrm{V}_{\text {SET }} \leq 1.5 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=\mathrm{V}_{\mathrm{CE}}=3.0 \mathrm{~V}$ <br> J/ K version <br> A/ C version <br> $B / D$ version | $\begin{aligned} & 144 \\ & 240 \\ & 400 \\ & \hline \end{aligned}$ | $\begin{array}{r} 180 \\ 300 \\ 500 \\ \hline \end{array}$ | $\begin{aligned} & 216 \\ & 360 \\ & 600 \\ & \hline \end{aligned}$ | kHz |
| $\begin{gathered} \Delta \text { foscl } \\ \Delta \mathrm{Ta} \\ \hline \end{gathered}$ | Oscillator Frequency Temperature Coefficient | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 85^{\circ} \mathrm{C}$ |  | $\pm 0.2$ |  | $\begin{aligned} & \% / \\ & { }^{\circ} \mathrm{C} \\ & \hline \end{aligned}$ |
| IDD1 | Supply Current 1 | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=\mathrm{V}_{\text {OUT }}=18.5 \mathrm{~V}$ <br> A/B/J/K version <br> C version <br> D version |  | $\begin{aligned} & 20 \\ & 30 \\ & 40 \\ & \hline \end{aligned}$ | $\begin{aligned} & 50 \\ & 60 \\ & 80 \\ & \hline \end{aligned}$ | $\mu \mathrm{A}$ |
| IstandBy | Standby Current | $\mathrm{V}_{\text {IN }}=18.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$, $\mathrm{V}_{\text {OUT }}=0 \mathrm{~V}$ |  | 0.0 | 0.5 | $\mu \mathrm{A}$ |
| IExth | EXT "H" Output Current | $\begin{aligned} & \mathrm{V}_{\text {IN }}=8 \mathrm{~V}, \mathrm{~V}_{\text {EXT }}=7.9 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=8 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}} \\ & =8 \mathrm{~V} \end{aligned}$ |  | -17 | -10 | mA |
| Iextl | EXT "L" Output Current | $\begin{aligned} & \mathrm{V}_{\text {IN }}=8 \mathrm{~V}, \mathrm{~V}_{\text {EXT }}=0.1 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}} \\ & =8 \mathrm{~V} \end{aligned}$ | 20 | 30 |  | mA |
| Isw | DLY switch current | $\mathrm{V}_{\text {IN }}=2.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{CE}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DLY}}=0.1 \mathrm{~V}$ | 1.0 | 2.0 |  | mA |
| $I_{\text {ceh }}$ | CE "H" Input Current | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=\mathrm{V}_{\text {OUT }}=18.5 \mathrm{~V}$ |  | 0.0 | 0.5 | $\mu \mathrm{A}$ |
| Icel | CE "L" Input Current | $\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {OUT }}=18.5 \mathrm{~V}, \mathrm{~V}_{\text {CE }}=0 \mathrm{~V}$ | -0.5 | 0.0 |  | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {ceh }}$ | CE "H" Input Voltage | $\mathrm{V}_{\text {IN }}=8 \mathrm{~V}$, $\mathrm{V}_{\text {OUt }}=0 \mathrm{~V}$ | 1.5 |  |  | V |
| $V_{\text {cel }}$ | CE "L" Input Voltage | $\mathrm{V}_{\text {IN }}=8 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=0 \mathrm{~V}$ |  |  | 0.3 | V |
| Dmax | Oscillator Maximum Duty Cycle |  | 100 |  |  | \% |
| DvFm | VFM Duty Cycle | A/B/J version |  | 35 |  | \% |
| Vuvlo1 | UVLO Voltage | $\mathrm{V}_{\text {OUT }}=0 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=2.5 \mathrm{~V} \rightarrow 1.5 \mathrm{~V}$ | 1.8 | 2.0 | 2.2 | V |
| V UVLO2 | UVLO Release Voltage | $\mathrm{V}_{\text {OUT }}=0 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=\mathrm{V}_{\text {CE }}=1.5 \mathrm{~V} \rightarrow 2.5 \mathrm{~V}$ |  | $\begin{array}{c\|} \hline \text { VuvLo1 } \\ +0.1 \end{array}$ | 2.3 | V |
| tstart | Soft-start Time | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=\mathrm{V}_{\mathrm{SET}}+1.5 \mathrm{~V}, \text { IoUT }=-10 \mathrm{~mA} \\ & \mathrm{~V}_{\mathrm{CE}}=0 \mathrm{~V} \rightarrow \mathrm{~V}_{\mathrm{SET}}+1.5 \mathrm{~V} \end{aligned}$ | 5 | 10 | 20 | ms |
| tprot | Protection Delay Time | $\begin{aligned} & \mathrm{V}_{\text {IN }}=\mathrm{V}_{\mathrm{CE}}=\mathrm{V}_{\mathrm{SET}}+1.5 \mathrm{~V} \\ & \mathrm{~V}_{\text {OUT }}=\mathrm{V}_{\mathrm{SET}}+1.5 \mathrm{~V} \rightarrow 0 \mathrm{~V} \end{aligned}$ | 10 | 20 | 35 | ms |

## TYPICAL APPLICATION AND APPLICATION HINTS



Typical Application

External Components

| Symbol | Description |
| :---: | :--- |
| PMOS | uPA1914, Renesas |
| L | CR105NP-270MC, Sumida |
| SD | CMS06, Toshiba |
| C1 | $10 \mu F$, Ceramic Type |
| C2 | $0.1 \mu \mathrm{~F}$, Ceramic Type |
| C4 | $47 \mu$ F, Tantalum Type |
| R1 | $0.02 \mu \mathrm{~F}$, Ceramic Type |

## TECHNICAL NOTES

- As shown in the block diagram, a parasitic diode is formed in each terminal, each of these diodes is not formed for load current, therefore do not use it in such a way. When you control the CE pin by another power supply, do not make its "H" level more than the voltage level of VIN pin.
- The operation of Latch-type protection circuit is as follows;

When the maximum duty cycle continues longer than the delay time for protection circuit, (Refer to the Electrical Characteristics) the protection circuit works to shutdown Power MOSFET with latching operation. Therefore when an input/output voltage difference is small, the protection circuit may work with small load current.
To release the protection of latch status, after disable this IC with a chip enable circuit, enable it again, or restart this IC with power-on. However, in the case of restarting this IC with power-on, after the power supply is turned off, if a certain amount of charge remains in $\mathrm{C}_{\mathrm{IN}}$, or some voltage is forced to $\mathrm{V}_{\text {in }}$ from $\mathrm{C}_{\mathrm{in}}$, this IC might not be restarted even after power-on.

- Set external components as close as possible to the IC and minimize the connection between the components and the IC. In particular, a capacitor should be connected to VOUT pin with the minimum connection. Make grounding sufficient and reinforce supplying. Large switching current flows through the connection of power line, an inductor and the connection of Vout. If the impedance of the connection of power supply is high, the voltage level of power supply of the IC fluctuates with the switching current. This may cause unstable operation of the IC.
- Use capacitors with a capacity of $22 \mu \mathrm{~F}$ or more for VOUT pin, and with good high frequency characteristics such as tantalum capacitors. We recommend to use capacitors with an allowable voltage which is at least twice as much as setting output voltage, in terms of the input capacitors, its voltage rating is twice or more than input voltage. This is because there may be a case where a spike-shaped high voltage is generated by an inductor when an external transistor is on and off.
- Choose an inductor that has sufficiently small D.C. resistance and large allowable current and is hard to reach magnetic saturation. If the value of inductance of an inductor is extremely small, the lıx may exceed the absolute maximum rating at the maximum loading. Use an inductor with appropriate inductance.
- Use a diode of a Schottky type with high switching speed, and also pay attention to its current capacity.
- Do not use this IC under the condition with Vin voltage at equal or less than minimum operating voltage.
- When the threshold level of an external power MOSFET is rather low and the drive-ability of voltage supplier is small, if the output pin is short circuit, input voltage may be equal or less than UVLO detector threshold. In this case, the devise is reset with UVLO function that is not the latch-protection function.
- With the PWM/VFM alternative circuit, when the on duty cycle of switching is $35 \%$ or less, the R1225N alters from PWM mode to VFM mode (Pulse skip mode). The purpose of this circuit is raising the efficiency with a light load by skipping the frequency and suppressing the consumption current. However, the ratio of output voltage against input voltage is $35 \%$ or less, ( $\mathrm{ex} . \mathrm{V}_{\text {IN }}>8.6 \mathrm{~V}$ and $\mathrm{V}_{\text {out }}=3.0 \mathrm{~V}$ ) even if the large current may be loaded, the IC keeps its VFM mode. As a result, frequency might be decreased, and oscillation waveform might be unstable. These phenomena are the typical characteristics of the IC with PWM/VFM alternative circuit.
$\star$ The performance of a power source circuit using this device is highly dependent on a peripheral circuit. A peripheral component or the device mounted on PCB should not exceed its rated voltage, rated current or rated power. When designing a peripheral circuit, please be fully aware of the following points.


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## HOW TO SET THE DELAY TIME FOR PROTECTION CIRCUIT

The equation describes how to calculate the delay time of protection circuit from the value of an external capacitor C4.
toly $=\mathrm{C} 4 \times 10^{6} \mathrm{sec}$ (in this equation, $1 \mu \mathrm{~F} \geq \mathrm{C} 4 \geq 1000 \mathrm{pF}$ )

Without the external capacitor, a certain delay time exists, therefore, if the external capacitor is less than 1000 pF , the error will increase. Further, if the external capacitor value is beyond $1 \mu \mathrm{~F}$, the time required to discharge the C 4 will be long, and this may cause the miss-operation. For example, if the protection circuit may work and released, soon after that the protection may work. In that case, C4 has not discharged completely yet, therefore, the delay time may be shorter than expected.


## OPERATION OF STEO-DOWN DCIDC CONVERTER AND OUTPUT CURRENT

The step-down DC/DC converter charges energy in the inductor when Lx transistor is ON, and discharges the energy from the inductor when Lx transistor is OFF and controls with less energy loss, so that a lower output voltage than the input voltage is obtained. The operation will be explained with reference to the following diagrams:


Basic Circuits


Current through L

Step 1: Lx Tr. turns on and current IL (= i1) flows, and energy is charged into CL. At this moment, IL increases from ILmin $(=0)$ to reach ILmax in proportion to the on-time period (ton) of LX Tr.
Step 2: When Lx Tr. turns off, Schottky diode (SD) turns on in order that L maintains IL at ILmax, and current IL (= i2) flows.
Step 3: IL decreases gradually and reaches ILmin after a time period of topen, and SD turns off, provided that in the continuous mode, next cycle starts before IL becomes to 0 because toff time is not enough. In this case, IL value is from this ILmin (>0).

In the case of PWM control system, the output voltage is maintained by controlling the on-time period (ton), with the oscillator frequency (fosc) being maintained constant.

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## Discontinuous Conduction Mode and Continuous Conduction Mode

The maximum value (ILmax) and the minimum value (ILmin) current which flow through the inductor is the same as those when Lx Tr. turns on and when it turns off.

The difference between ILmax and ILmin, which is represented by $\Delta l$;
$\Delta I=\operatorname{llmax}-\operatorname{llmin}=\mathrm{V}_{\text {out }} \mathrm{x}$ topen $/ \mathrm{L}=\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {out }}\right) \times$ ton $/ \mathrm{L}$ $\qquad$ Equation 1

Where, $\mathrm{T}=1 / \mathrm{fosc}=$ ton + toff
Duty (\%) = ton $/ \mathrm{T} \times 100=$ ton $\times$ fosc $\times 100$
topen $\leq$ toff

In Equation 1, Vout $x$ topen / $L$ and $\left(V_{I N}-V_{\text {Out }}\right) x$ ton / $L$ are respectively shown the change of the current at ON, and the change of the current at OFF.
When the output current (lout) is relatively small, topen < toff as illustrated in the above diagram. In this case, the energy is charged in the inductor during the time period of ton and is discharged in its entirely during the time period of toff, therefore ILmin becomes to zero (ILmin = 0). When lout is gradually increased, eventually, topen becomes to toff (topen = toff), and when lout is further increased, ILmin becomes larger than zero (ILmin $>0$ ). The former mode is referred to as the discontinuous mode and the latter mode is referred to as continuous mode.

In the continuous mode, when Equation 1 is solved for ton and assumed that the solution is tonc,
tonc $=T \times V_{\text {out }} / V_{\text {IN }}$ $\qquad$ Equation 2

When ton < tonc, the mode is the discontinuous mode, and when ton = tonc, the mode is the continuous mode.

## OUTPUT CURRENT AND SELECTION OF EXTERNAL COMPONENTS

When Lx Tr. is "ON":
(Wherein, Ripple Current P-P value is described as $I_{R P}$, ON resistance of $L X$ Tr. is described as $R_{P}$ the direct current of the inductor is described as RL.)
$V_{I N}=V_{\text {OUT }}+\left(R_{P}+R_{L}\right) \times$ lout $+L \times I_{\text {RP }} /$ ton $\qquad$ Equation 3

When Lx Tr. is "OFF":
$\mathrm{L} \times \mathrm{I}_{\mathrm{RP}} /$ toff $=\mathrm{V}_{\mathrm{F}}+\mathrm{V}_{\text {OUt }}+\mathrm{R} \mathrm{L} \times$ lout.
Equation 4

Put Equation 4 to Equation 3 and solve for ON duty, ton $/($ toff + ton $)=$ Don,

Don $=\left(V_{\text {OUT }}+V_{F}+R_{L} \times\right.$ loUt $) /\left(V_{\text {IN }}+V_{F}-R_{\text {P }} \times\right.$ lout $)$ $\qquad$ Equation 5

Ripple Current is as follows;
$I_{\text {RP }}=\left(V_{\text {IN }}-V_{\text {OUT }}-R_{P} \times\right.$ lout $-R_{L} \times$ lout $) \times D_{\text {ON }} / f / L$ $\qquad$ Equation 6

Wherein, peak current that flows through L, Lx Tr., and SD is as follows;
$\mathrm{ILmax}=\mathrm{l}_{\mathrm{OUT}}+\mathrm{I}_{\mathrm{RP}} / 2$ $\qquad$ Equation 7

Consider ILmax, condition of input and output and select external components.
$\star$ The above explanation is directed to the calculation in an ideal case in continuous mode.

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## EXTERNAL COMPONENTS

1. Inductor

Select an inductor that peak current does not exceed ILmax. If larger current than allowable current flows, magnetic saturation occurs and make transform efficiency worse. When the load current is definite, the smaller value of $L$, the larger the ripple current. Provided that the allowable current is large in that case and DC current is small, therefore, for large output current, efficiency is better than using an inductor with a large value of $L$ and vice versa.
2. Diode

Use a diode with low $V_{F}$ (Schottky type is recommended.) and high switching speed. Reverse voltage rating should be more than $\mathrm{V}_{\mathrm{IN}}$ and current rating should be equal or more than ILmax.
3. Capacitors

As for $C_{i N}$, use a capacitor with low ESR (Equivalent Series Resistance) and a capacity of at least $10 \mu \mathrm{~F}$ for stable operation. Cout can reduce ripple of Output Voltage, therefore $47 \mu \mathrm{~F}$ or more value of tantalum type capacitor is recommended.
4.Lx Transistor

Pch Power MOSFET is required for this IC. Its breakdown voltage between gate and source should be a few $V$ higher than Input Voltage. In the case of Input Voltage is low, to turn on MOSFET completely, to use a MOSFET with low threshold voltage is effective. If a large load current is necessary for your application and important, choose a MOSFET with low ON resistance for good efficiency. If a small load current is mainly necessary for your application, choose a MOSFET with low gate capacity for good efficiency. Maximum continuous drain current of MOSFET should be larger than peak current, ILmax.

## TIMING CHART

Case 1. Set Vout Voltage > 2.1 V (Set Vout Voltage > UVLO Voltage)


The timing chart shown above describes the changing process of input voltage rising, stable operating, operating with large current, reset with CE pin, stable operating, input voltage falling, input voltage recovering, and stable operating.
First, until when the input voltage ( V IN ) reaches the set output voltage, the circuit inside keeps the condition of pre-standby.
Second, after $\mathrm{V}_{\mathrm{IN}}$ becomes beyond the set output voltage, soft-start operation starts, when the soft-start operation finishes, the operation becomes stable.
If too large current flows through the circuit because of short or other reasons, EXT signal ignores that during the delay time of protection circuit. (The current value depends on the circuit.)
After the delay time passes, the latch protection works, or EXT signal will be " H ", then output will turn off. To release the latch protection, input voltage should be equal or lower than UVLO level, or restart with CE (Once turn off the circuit with CE and turn it on again). In the timing charge above, release the latch function is realized with CE signal from "L" to "H". After removing the cause of large current and the reset with CE, soft-start operation starts and after the soft-start time, the operation will be back to stable.
If the $\mathrm{V}_{\mathrm{IN}}$ becomes lower than the set Vout, that situation is same as large current condition, so protection circuit may be ready to work, therefore, after the delay time of protection circuit, EXT will be "H" and the output turns off.
Further, if the $\mathrm{V}_{\mathrm{IN}}$ is lower than UVLO voltage, the circuit inside will be stopped by UVLO function. After that, if $\mathrm{V}_{\text {IN }}$ rises, until when the $\mathrm{V}_{\text {IN }}$ reaches the set output voltage, the circuit inside keeps the condition of pre-standby. Then after $V_{I N}$ becomes beyond the set output voltage, soft-start operation starts, when the soft-start operation finishes, the operation becomes stable.

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Case 2. Set Vout Voltage $\leq 2.0$ V (Set Vout Voltage < UVLO Voltage)


The timing chart shown above describes the changing process of input voltage rising, stable operating, operating with large current, reset with CE pin, stable operating, input voltage falling, input voltage recovering, and stable operating.

First, until when the input voltage $(\mathrm{V} / \mathrm{IN})$ reaches the UVLO voltage, the circuit inside keeps the condition of prestandby. Second, after VIN becomes beyond the UVLO voltage, soft-start operation starts, when the soft-start operation finishes, the operation becomes stable. If too large current flows through the circuit because of short or other reasons, EXT signal ignores that during the delay time of protection circuit. (The current value depends on the circuit.) After the delay time passes, the latch protection works, or EXT signal will be " H ", then output will turn off. To release the latch protection, input voltage should be equal or lower than UVLO level, or restart with CE (Once turn off the circuit with CE and turn it on again). In the timing charge above, release the latch function is realized with CE signal from "L" to "H". After removing the cause of large current and the reset with CE, soft-start operation starts and after the soft-start time, the operation will be back to stable. Further, if the Vin is lower than UVLO voltage, the circuit inside will be stopped by UVLO function. After that, if Vin rises, until when the $\mathrm{V}_{\text {IN }}$ reaches UVLO voltage, the circuit inside keeps the condition of pre-standby. Then after $\mathrm{V}_{\text {IN }}$ becomes beyond the UVLO voltage, soft-start operation starts, when the soft-start operation finishes, the operation becomes stable.

## TEST CIRCUITS


A) Output Voltage, Oscillator Frequency, CE "H" Input Voltage, CE "L" Input Voltage, Soft-start time

B) Supply Current 1

D) EXT "H" Output Current
F) DLY Switching Current


C) Standby Current

E) EXT "L" Output Current
 Current

H) Output Delay Time for Protection Circuit

External Components

| Symbol | Description |
| :---: | :--- |
| PMOS | Pch Power MOS, Hitachi: HAT1020R |
| L1 | $27 \mu \mathrm{H}$, Sumida: CD104NP-270MC |
| D1 | Schottky Type, ROHM: RB491D |
| C1 | $47 \mu \mathrm{~F}$, Tantalum Type |
| C2 | $47 \mu \mathrm{~F}$, Tantalum Type |
| C3 | $0.02 \mu \mathrm{~F}$, Ceramic Type |

## TYPICAL CHARACTERISTICS

1) Efficiency vs. Output Current






































R1225N502D (Vin=6.5V) CDRH127-10 $\mu \mathrm{H}$






2) Ripple Voltage vs. Output Current

















3) Input Voltage vs. Output Voltage


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4) Output Voltage vs. Output Current

















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5) Load Transient Response








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11. Please contact Ricoh sales representatives should you have any questions or comments concerning the products or the technical information.

Ricoh is committed to reducing the environmental loading materials in electrical devices with a view to contributing to the protection of human health and the environment.
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