

# **TS2012EI**

**Datasheet** - **production data**

# Filter-free Flip Chip stereo 2 x 2.5 W class D audio power amplifier

**G1 INL+ LIN+ LIN- RIN- RIN+** PVCC **PVCC co c G0 c AVCC LOUT+ STDBYR AGND ROUT+ LOUT- STDBYL PGND ROUT-Flip Chip 16 Pin connection (top view)**

### **Features**

- Operates from  $V_{CC} = 2.5$  to 5.5 V
- Dedicated standby mode active low for each channel
- Output power per channel: 1.15 W at 5 V or 0.63 W at 3.6 V into 8  $\Omega$  with 1% THD+N max.
- Output power per channel: 1.85 W at 5 V into  $4 \Omega$  with 1% THD+N max.
- Output short-circuit protection
- Four gain setting steps: 6, 12, 18, 24 dB
- Low current consumption
- PSSR: 63 dB typ. at 217 Hz.
- Fast startup phase: 7.8 ms
- Thermal shutdown protection
- Flip Chip 16 bump lead-free package

# **Applications** Cellular phones

PDA

## **Description**

The TS2012EI is a fully-differential stereo class D power amplifier able to drive up to 1.15 W into an  $8 \Omega$  load at 5 V per channel. It achieves better efficiency compared to typical class AB audio amps.

The device has four different gain settings utilizing two digital pins: G0 and G1.

Pop and click reduction circuitry provides low on/off switch noise while allowing the device to start within 8 ms.

Two standby pins (active low) allow each channel to be switched off separately.

The TS2012EI is available in a Flip Chip 16 bump lead-free package.

#### **Table 1. Device summary**



April 2014 **DociD026152 Rev 1** 2014 **DociD026152 Rev 1** 

This is information on a product in full production.

# **Contents**





# <span id="page-2-0"></span>**1 Absolute maximum ratings and operating conditions**





1. All voltage values are measured with respect to the ground pin.

2. The magnitude of the input signal must never exceed  $V_{CC}$  + 0.3 V / GND - 0.3 V.

- 3. The device is protected in case of over temperature by a thermal shutdown active at 150°C.
- 4. Exceeding the power derating curves during a long period will cause abnormal operation.
- 5. Human body model: 100 pF discharged through a 1.5 k $\Omega$  resistor between two pins of the device, done for all couples of pin combinations with other pins floating.
- 6. Machine model: a 200 pF cap is charged to the specified voltage, then discharged directly between two pins of the device with no external series resistor (internal resistor < 5  $\Omega$ ), done for all couples of pin combinations with other pins floating.
- 7. Implemented short-circuit protection protects the amplifier against damage by short-circuit between positive and negative outputs of each channel and between outputs and ground.



<span id="page-3-0"></span>

Symbol	<b>Parameter</b>	Value	Unit
$V_{\rm CC}$	Supply voltage	2.5 to $5.5$	V
$V_{in}$	Input voltage range	GND to $V_{CC}$	$\vee$
$V_{ic}$	Input common mode voltage <sup>(1)</sup>	GND+0.5V to $V_{CC}$ -0.9V	V
<b>V<sub>STBY</sub></b>	Standby voltage input (2) Device ON Device in STANDBY <sup>(3)</sup>	$1.4 \leq V_{STBY} \leq V_{CC}$ GND $\leq$ V <sub>STBY</sub> $\leq$ 0.4	$\vee$
$R_L$	Load resistor	>4	Ω
$V_{\text{IH}}$	GO, G1 - high level input voltage <sup>(4)</sup>	1.4 $\leq$ $V_{\text{IH}} \leq$ $V_{\text{CC}}$	V
$V_{IL}$	GO, G1 - low level input voltage	GND $\leq$ V <sub>II</sub> $\leq$ 0.4	$\vee$
$R_{thja}$	Thermal resistance junction to ambient (5)	90	°C/W

**Table 3. Operating conditions**

1. I V<sub>oo</sub> I  $\leq 40$  mV max with all differential gains except 24 dB. For 24 dB gain, input decoupling capacitors are mandatory.

2. Without any signal on standby pin, the device is in standby (internal 300 k $\Omega$  +/-20% pull-down resistor).

3. Minimum current consumption is obtained when  $V_{STBY} = GND$ .

4. Between G0, G1pins and <sub>GND</sub>, there is an internal 300 k $\Omega$  (+/-20%) pull-down resistor. When pins are floating, the gain is 6 dB. In full standby (left and right channels OFF), these resistors are disconnected (HiZ input).

5. With a 4-layer PCB.



# <span id="page-4-0"></span>**2 Typical application**

<span id="page-4-1"></span>







**Table 5. Pin description**



# **Table 4. External component description**



# <span id="page-6-0"></span>**3 Electrical characteristics**

# <span id="page-6-1"></span>**3.1 Electrical characteristics tables**

#### Table 6. V<sub>CC</sub> = +5 V, GND = 0 V, V<sub>ic</sub> = 2.5 V, T<sub>amb</sub> = 25° C (unless otherwise specified)

<span id="page-6-2"></span>





# Table 6.  $V_{CC}$  = +5 V, GND = 0 V, V<sub>ic</sub> = 2.5 V, T<sub>amb</sub> = 25° C (unless otherwise specified) (continued)

1. Dynamic measurements - 20\*log(rms( $V_{\text{out}}$ )/rms( $V_{\text{right}}$ )).  $V_{\text{right}}$  is the superimposed sinus signal to  $V_{\text{CC}}$  at f = 217 Hz.

2. See *Section 4.6: Wake-up time*  $(t_{WU})$  *and shutdown time*  $(t_{STBY})$  *on page 23.* 











# Table 7.  $V_{CC}$  = +3.6 V, GND = 0 V, V<sub>ic</sub> = 1.8V, T<sub>amb</sub> = 25° C (unless otherwise specified) (continued)

1. Dynamic measurements - 20\*log(rms( $V_{out}$ )/rms( $V_{right}$ )).  $V_{right}$  is the superimposed sinus signal to  $V_{CC}$  at f = 217 Hz.

2. See *Section 4.6: Wake-up time*  $(t_{WU})$  *and shutdown time*  $(t_{STBY})$  *on page 23.* 





<span id="page-10-0"></span>

<b>Symbol</b>	<b>Parameter</b>	Min.	Typ.	Max.	Unit
$I_{\rm CC}$	Supply current No input signal, no load, both channels		2.8	4	mA
$I_{STBY}$	Standby current No input signal, $V_{STBY}$ = GND		0.45	2	μA
$V_{00}$	Output offset voltage Floating inputs, G = 6 dB, R <sub>1</sub> = 8 $\Omega$			25	mV
$\mathsf{P}_\mathsf{O}$	Output power THD + N = 1% max, f = 1 kHz, R <sub>1</sub> = 4 $\Omega$ THD + N = 1% max, f = 1 kHz, $R_1$ = 8 $\Omega$ THD + N = 10% max, f = 1 kHz, R <sub>1</sub> = 4 $\Omega$ THD + N = 10% max, f = 1 kHz, $R_L$ = 8 $\Omega$		0.45 0.3 0.6 0.38		W
$THD + N$	Total harmonic distortion + noise $P_0 = 0.2$ W, G = 6 dB, f = 1 kHz, R <sub>L</sub> = 8 $\Omega$		0.2		$\%$
Efficiency	Efficiency per channel $P_0 = 0.45$ W, R <sub>1</sub> = 4 $\Omega$ + 15 µH $P_0 = 0.3$ W, $R_L = 8 \Omega + 15$ µH		78 87		$\%$
<b>PSRR</b>	Power supply rejection ratio with inputs grounded $C_{in}$ = 1 µF <sup>(1)</sup> , f = 217 Hz, R <sub>L</sub> = 8 $\Omega$ , Gain = 6 dB, $V_{\text{ripole}}$ = 200 m $V_{\text{pp}}$		65		dB
Crosstalk	Channel separation $G = 6$ dB, f = 1 kHz, R <sub>L</sub> = 8 $\Omega$		90		
<b>CMRR</b>	Common mode rejection ratio $C_{in}$ = 1 µF, f = 217 Hz, R <sub>L</sub> = 8 $\Omega$ , Gain = 6 dB, $\Delta_{\text{VICM}}$ = 200 mV <sub>pp</sub>		62		dB
Gain	Gain value with no load $G1 = G0 = V_{  }$ $G1 = V_{II}$ and $G0 = V_{IH}$ G1 = $V_{\text{IH}}$ and G0 = $V_{\text{IL}}$ $G1 = G0 = V_{IH}$	5.5 11.5 17.5 23.5	6 12 18 24	6.5 12.5 18.5 24.5	dΒ
$Z_{in}$	Single-ended input impedance Referred to ground $Gain = 6 dB$ $Gain = 12 dB$ $Gain = 18 dB$ $Gain = 24 dB$	24 24 12 6	30 30 15 7.5	36 36 18 9	$k\Omega$
F <sub>PWM</sub>	Pulse width modulator base frequency	190	280	370	kHz
<b>SNR</b>	Signal-to-noise ratio (A-weighting) $P_0 = 0.28$ W, G = 6 dB, R <sub>L</sub> = 8 $\Omega$		93		dB
t <sub>WU</sub>	Total wake-up time <sup>(2)</sup>	$\mathbf{3}$	7.8	12	ms

Table 8.  $V_{CC}$  = +2.5 V, GND = 0 V, V<sub>ic</sub> = 1.25 V, T<sub>amb</sub> = 25 °C (unless otherwise specified)





# Table 8.  $V_{CC}$  = +2.5 V, GND = 0 V, V<sub>ic</sub> = 1.25 V, T<sub>amb</sub> = 25 °C (unless otherwise specified) (continued)

1. Dynamic measurements - 20\*log(rms( $V_{out}$ )/rms( $V_{right}$ )).  $V_{right}$  is the superimposed sinus signal to  $V_{CC}$  at f = 217 Hz.

2. See *Section 4.6: Wake-up time*  $(t_{WU})$  *and shutdown time*  $(t_{STBY})$  *on page 23.* 





## <span id="page-12-0"></span>**3.2 Electrical characteristic curves**

The graphs shown in this section use the following abbreviations.

- $R_L$ + 15 µH or 30 µH = pure resistor + very low series resistance inductor.
- Filter = LC output filter (1  $\mu$ F+ 30  $\mu$ H for 4  $\Omega$  and 0.5  $\mu$ F+15  $\mu$ H for 8  $\Omega$ ).

All measurements are done with  $C_{S1}=1 \mu F$  and  $C_{S2}=100 \text{ nF}$  (*[Figure 2](#page-12-1)*), except for the PSRR where C<sub>S1</sub> is removed (*[Figure 3](#page-13-0)*).

<span id="page-12-1"></span>

**Figure 2. Test diagram for measurements**



<span id="page-13-0"></span>





#### **Figure 4. Current consumption vs. power supply voltage**



**Figure 6. Efficiency vs. output power (one channel)**



#### **Figure 8. Efficiency vs. output power (one channel)**

#### **Figure 9. Efficiency vs. output power (one channel)**





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#### **Figure 5. Current consumption vs. standby voltage (one channel)**



**Figure 7. Efficiency vs. output power (one channel)**



#### **Figure 11. Efficiency vs. output power (one channel)**

**Figure 12. PSRR vs. frequency Figure 13. PSRR vs. frequency**

**Figure 10. Efficiency vs. output power**





Figure 15. PSRR vs. common mode input **voltage**







#### **Figure 16. PSRR vs. common mode input voltage**

#### **Figure 17. PSRR vs. common mode input voltage**









**Figure 20. CMRR vs. frequency Figure 21. CMRR vs. common mode input voltage**





Vripple = 200mVpp  $F = 217$ Hz,  $G = +12$ dB  $RL = 8\Omega + 15\mu H$ Tamb =  $25^{\circ}$ C

 $\overline{\text{Vcc}=2.5\text{V}}$ 

≍ չ

-90 -80 -70 -60 -50 -40  $-30$ -20 -10 0

**CMRR (dB)**

 $CMRR$  (dB)

 $Vcc=3.6V$ 





**Figure 25. THD+N vs. output power**

**Figure 24. CMRR vs. common mode input voltage**

**Common Mode Input Voltage (V)**



 $\sqrt{\text{Vcc}=5V}$ 





TШ

Ш



**voltage**





Figure 30. Crosstalk vs. frequency Figure 31. Output power vs. power supply **voltage**



**Figure 32. Output power vs. power supply voltage**

**Figure 33. Power derating curves**





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#### **Figure 34. Startup and shutdown phase**   $V_{CC}$  = 5 V, G = 6 dB, C<sub>in</sub> = 1 µF, inputs grounded

#### **Figure 35. Startup and shutdown phase**   $V_{CC}$  = 5 V, G = 6 dB, C<sub>in</sub> = 1 µF, V<sub>in</sub> = 2 V<sub>pp</sub>, **F = 500 Hz**





# <span id="page-20-0"></span>**4 Application information**

# <span id="page-20-1"></span>**4.1 Differential configuration principle**

The TS2012EI is a monolithic fully-differential input/output class D power amplifier. The TS2012EI also includes a common-mode feedback loop that controls the output bias value to average it at  $V_{CC}/2$  for any DC common mode input voltage. This allows the device to always have a maximum output voltage swing, and by consequence, maximize the output power. Moreover, as the load is connected differentially compared with a single-ended topology, the output is four times higher for the same power supply voltage.

The **advantages** of a full-differential amplifier are:

- high PSRR (power supply rejection ratio),
- high common mode noise rejection,
- virtually zero pop without additional circuitry, giving a faster start-up time compared to conventional single-ended input amplifiers,
- easier interfacing with differential output audio DACs,
- no input coupling capacitors required thanks to the common mode feedback loop.

## <span id="page-20-2"></span>**4.2 Gain settings**

In the flat region of the frequency-response curve (no input coupling capacitor or internal feedback loop + load effect), the differential gain can be set to 6, 12 18, or 24 dB, depending on the logic level of the G0 and G1 pins, as shown in *[Table 9](#page-20-4)*.

<span id="page-20-4"></span>

rapio or Sam comingo with Solaria St. pino									
G1	G <sub>0</sub>	Gain (dB)	Gain (V/V)						
		12							
		18							
		24	16						

**Table 9. Gain settings with G0 and G1 pins**

*Note:* Between pins G0, G1 and GND there is an internal 300 k $\Omega$  (+/-20%) resistor. When the pins *are floating, the gain is 6 dB. In full standby (left and right channels OFF), these resistors are disconnected (HiZ input).*

# <span id="page-20-3"></span>**4.3 Common mode feedback loop limitations**

As explained previously, the common mode feedback loop allows the output DC bias voltage to be averaged at  $V_{\rm CC}/2$  for any DC common mode bias input voltage.

Due to the Vic limitation of the input stage (see *[Table 3: Operating conditions on page 4](#page-3-0)*), the common mode feedback loop can fulfill its role only within the defined range.



<span id="page-21-0"></span>If a low frequency bandwidth limitation is required, it is possible to use input coupling capacitors. In the low-frequency region, the input coupling capacitor  $C_{in}$  starts to have an effect.  $C_{in}$  forms, with the input impedance  $Z_{in}$ , a first order high-pass filter with a -3 dB cutoff frequency (see *[Table 6](#page-6-2)* to *[Table 8](#page-10-0)*).

$$
F_{CL} = \frac{1}{2 \cdot \pi \cdot Z_{in} \cdot C_{in}}
$$

So, for a desired cut-off frequency  $F_{CL}$ ,  $C_{in}$  is calculated as follows.

$$
C_{in} = \frac{1}{2 \cdot \pi \cdot Z_{in} \cdot F_{CL}}
$$

with F<sub>CL</sub> in Hz,  $Z_{in}$  in  $\Omega$  and  $C_{in}$  in F.

The input impedance  $Z_{in}$  is for the whole power supply voltage range and it changes with the gain setting. There is also a tolerance around the typical values (see *[Table 6](#page-6-2)* to *[Table 8](#page-10-0)*).



**Figure 36. Cut-off frequency vs. input capacitor**



### <span id="page-22-0"></span>**4.5 Decoupling of the circuit**

Power supply capacitors, referred to as  $C_{S1}$  and  $C_{S2}$ , are needed to correctly bypass the TS2012EI.

The TS2012EI has a typical switching frequency of 280 kHz and an output fall and rise time of approximately 5 ns. Due to these very fast transients, careful decoupling is mandatory.

A 1  $\mu$ F ceramic capacitor (C<sub>S1</sub>) between PVCC and PGND and one additional ceramic capacitor 0.1  $\mu$ F (C<sub>S2</sub>) are enough. A 1  $\mu$ F capacitor must be located as close as possible to the device PVCC pin in order to avoid any extra parasitic inductance or resistance created by a long track wire. Parasitic loop inductance, in relation with di/dt, introduces overvoltage that decreases the global efficiency of the device and may cause, if this parasitic inductance is too high, a breakdown of the TS2012EI. For filtering low-frequency noise signals on the power line, you can use a  $C_{S1}$  capacitor of 4.7  $\mu$ F or more.

In addition, even if a ceramic capacitor has an adequate high frequency ESR (equivalent series resistance) value, its current capability is also important. A size of 0603 is a good compromise, particularly when a 4  $\Omega$  load is used.

Another important parameter is the rated voltage of the capacitor. A 1  $\mu$ F/6.3 V capacitor used at 5 V, loses about 50% of its value. With a power supply voltage of 5 V, the decoupling value, instead of 1 µF, could be reduced to 0.5 µF. As  $C<sub>S</sub>$  has particular influence on the THD+N in the medium-to-high frequency region, this capacitor variation becomes decisive. In addition, less decoupling means higher overshoots, which can be problematic if they reach the power supply AMR value (6 V).

# <span id="page-22-1"></span>**4.6** Wake-up time (t<sub>WU</sub>) and shutdown time (t<sub>STBY</sub>)

During the wake-up sequence when the standby is released to set the device ON, there is a delay. The wake-up sequence of the TS2012EI consists of two phases. During the first phase  $t_{WU-A}$ , a digitally-generated delay, mutes the outputs. Then, the gain increasing phase  $t_{WU-A}$  begins. The gain increases smoothly from the mute state to the preset gain selected by the digital pins G0 and G1. This startup sequence avoids any pop noise during startup of the amplifier. Refer to *[Figure 37: Wake-up phase](#page-23-0)*



<span id="page-23-0"></span>

When the standby command is set, the time required to set the output stage to high impedance and to put the internal circuitry in shutdown mode is called the standby time. This time is used to decrease the gain from its nominal value set by the digital pins G0 and G1 to mute and avoid any pop noise during shutdown. The gain decreases smoothly until the outputs are muted (*[Figure 38](#page-23-1)*).

<span id="page-23-1"></span>

**Figure 38. Shutdown phase**



## <span id="page-24-0"></span>**4.7 Consumption in shutdown mode**

Between the shutdown pin and GND there is an internal 300 k $\Omega$  (+-/20%) resistor. This resistor forces the TS2012EI to be in shutdown when the shutdown input is left floating.

However, this resistor also introduces additional shutdown power consumption if the shutdown pin voltage is not at 0 V.

With a 0.4 V shutdown voltage pin for example, you must add 0.4 V/300 k $\Omega$  = 1.3 µA typical (0.4 V/240 k $\Omega$  = 1.66 µA maximum) for each shutdown pin to the standby current specified in *[Table 6](#page-6-2)* to *[Table 8](#page-10-0)*. Of course, this current will be provided by the external control device for the standby pins.

# <span id="page-24-1"></span>**4.8 Single-ended input configuration**

It is possible to use the TS2012EI in a single-ended input configuration. However, input coupling capacitors are mandatory in this configuration. *[Figure 39](#page-24-2)* shows a typical singleended input application.

<span id="page-24-2"></span>

**Figure 39. Typical application for single-ended input configuration**



### <span id="page-25-0"></span>**4.9 Output filter considerations**

The TS2012EI is designed to operate without an output filter. However, due to very sharp transients on the TS2012EI output, EMI-radiated emissions may cause some standard compliance issues.

These EMI standard compliance issues can appear if the distance between the TS2012EI outputs and loudspeaker terminal are long (typically more than 50 mm, or 100 mm in both directions, to the speaker terminals). Because the PCB layout and internal equipment device are different for each configuration, it is difficult to provide a one-size-fits-all solution.

However, to decrease the probability of EMI issues, there are several simple rules to follow.

- Reduce, as much as possible, the distance between the TS2012EI output pins and the speaker terminals.
- Use a ground plane to "shield" sensitive wires.
- Place, as close as possible to the TS2012EI and in series with each output, a ferrite bead with a rated current of at least 2.5 A and an impedance greater than 50  $\Omega$  at frequencies above 30 MHz. If, after testing, these ferrite beads are not necessary, replace them by a short-circuit.
- Allow extra footprint to place, if necessary, a capacitor to short perturbations to ground (*[Figure 40](#page-25-2)*).

<span id="page-25-2"></span>

#### **Figure 40. Ferrite chip bead placement**

In the case where the distance between the TS2012EI output and the speaker terminals is too long, it is possible to have low frequency EMI issues due to the fact that the typical operating frequency is 280 kHz. In this configuration, it is necessary to use the output filter represented in *[Figure 1 on page 5](#page-4-1)* as close as possible to the TS2012EI.

# <span id="page-25-1"></span>**4.10 Short-circuit protection**

The TS2012EI includes output short-circuit protection. This protection prevents the device from being damaged in case of fault conditions on the amplifier outputs.

When a channel is in operating mode and a short-circuit occurs between two outputs of the channel or between an output and ground, the short-circuit protection detects this situation and puts the appropriate channel into standby. To put the channel back into operating mode, it is necessary to put the channel's standby pin to logical LO, and then back again to logical HI and wake up the channel.



# <span id="page-26-0"></span>**4.11 Thermal shutdown**

The TS2012EI device has an internal thermal shutdown protection in the event of extreme temperatures to protect the device from overheating. Thermal shutdown is active when the device reaches 150° C. When the temperature decreases to safe levels, the circuit switches back to normal operation.



# <span id="page-27-0"></span>**5 Package information**

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK® packages, depending on their level of environmental compliance. ECOPACK® specifications, grade definitions and product status are available at: *[www.st.com](http://www.st.com)*. ECOPACK® is an ST trademark.









#### **Figure 43. Marking (top view)**







**Figure 45. Recommended footprint**





# <span id="page-30-0"></span>**6 Revision history**







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info@moschip.ru

 $\circled{1}$  +7 495 668 12 70

Общество с ограниченной ответственностью «МосЧип» ИНН 7719860671 / КПП 771901001 Адрес: 105318, г.Москва, ул.Щербаковская д.3, офис 1107

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105318, г.Москва, ул.Щербаковская д.3, офис 1107, 1118, ДЦ «Щербаковский»

Телефон: +7 495 668-12-70 (многоканальный)

Факс: +7 495 668-12-70 (доб.304)

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Skype отдела продаж: moschip.ru moschip.ru\_4

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