## Data Sheet

## FEATURES

Single-channel, 1024-position resolution $20 \mathrm{k} \Omega, 50 \mathrm{k} \Omega$, and $100 \mathrm{k} \Omega$ nominal resistance Calibrated 1\% nominal resistor tolerance (resistor performance mode)
Rheostat mode temperature coefficient: $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ Voltage divider temperature coefficient: $5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$
Single-supply operation: 9 V to 33 V
Dual-supply operation: $\pm 9 \mathrm{~V}$ to $\pm 16.5 \mathrm{~V}$
SPI-compatible serial interface
Wiper setting readback

## APPLICATIONS

Mechanical potentiometer replacement Instrumentation: gain and offset adjustment Programmable voltage-to-current conversion Programmable filters, delays, and time constants Programmable power supply Low resolution DAC replacements

## Sensor calibration

## GENERAL DESCRIPTION

The AD5293 is a single-channel, 1024-position digital potentiometer (in this data sheet, the terms digital potentiometer and RDAC are used interchangeably) with a $<1 \%$ end-to-end resistor tolerance error. The AD5293 performs the same electronic adjustment function as a mechanical potentiometer with enhanced resolution, solid state reliability, and superior low temperature coefficient performance. This device is capable of operating at high voltages and supporting both dual-supply operation at $\pm 10.5 \mathrm{~V}$ to $\pm 15 \mathrm{~V}$ and single-supply operation at 21 V to 30 V .


The AD5293 offers guaranteed industry-leading low resistor tolerance errors of $\pm 1 \%$ with a nominal temperature coefficient of $35 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$. The low resistor tolerance feature simplifies openloop applications as well as precision calibration and tolerance matching applications.

The AD5293 is available in a compact 14-lead TSSOP package. The part is guaranteed to operate over the extended industrial temperature range of $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$.

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## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS— $\mathbf{2 0} \mathbf{~ k} \Omega$ VERSIONS

$\mathrm{V}_{\mathrm{DD}}=21 \mathrm{~V}$ to $33 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=0 \mathrm{~V} ; \mathrm{V}_{\mathrm{DD}}=10.5 \mathrm{~V}$ to 16.5 V , $\mathrm{V}_{\mathrm{SS}}=-10.5 \mathrm{~V}$ to $-16.5 \mathrm{~V} ; \mathrm{V}_{\text {Logic }}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{DD}}, \mathrm{V}_{\mathrm{B}}=\mathrm{V}_{\mathrm{SS}}$, $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+105^{\circ} \mathrm{C}$, unless otherwise noted.

Table 1.


| Parameter | Symbol | Conditions | Min | Typ ${ }^{1}$ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC CHARACTERISTICS4,8 |  |  |  |  |  |  |
| Bandwidth | BW | -3 dB |  | 520 |  | kHz |
| Total Harmonic Distortion | THDw | $\mathrm{V}_{\mathrm{A}}=1 \mathrm{Vrms}, \mathrm{V}_{\mathrm{B}}=0 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$, |  | -93 |  | dB |
| Vw Settling Time |  | $\begin{aligned} & \mathrm{V}_{\mathrm{A}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{B}}=0 \mathrm{~V}, \pm 0.5 \mathrm{LSB} \text { error } \\ & \text { band, initial code }=\text { zero scale } \end{aligned}$ |  |  |  |  |
|  |  | Code = full scale, R-normal mode |  | 750 |  | ns |
|  |  | Code = full scale, R-perf mode |  | 2.5 |  |  |
|  |  | Code = half scale, R-normal mode |  | 2.5 |  |  |
|  |  | Code $=$ half scale, R -perf mode |  | 5 |  |  |
| Resistor Noise Density | $\mathrm{e}_{\text {N_wb }}$ | $\begin{aligned} & \mathrm{RwB}=10 \mathrm{k} \Omega, \mathrm{~T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \\ & 0 \mathrm{kHz} \text { to } 200 \mathrm{kHz} \end{aligned}$ |  | 10 |  | $\mathrm{nV} / \sqrt{\mathrm{Hz}}$ |

${ }^{1}$ Typicals represent average readings at $25^{\circ} \mathrm{C} ; \mathrm{V}_{\mathrm{DD}}=+15 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=-15 \mathrm{~V}$, and $\mathrm{V}_{\text {LOGIC }}=5 \mathrm{~V}$.
${ }^{2}$ Resistor position nonlinearity error. R-INL is the deviation from an ideal value measured between Rws at Code $0 \times 00 B$ to Code $0 \times 3 F F$ or between Rwa at Code $0 \times 3 F 3$ to Code $0 \times 000$. R-DNL measures the relative step change from ideal between successive tap positions. The specification is guaranteed in resistor performance mode with a wiper current of 1 mA for $\mathrm{V}_{\mathrm{A}}<12 \mathrm{~V}$ and 1.2 mA for $\mathrm{V}_{\mathrm{A}} \geq 12 \mathrm{~V}$.
${ }^{3}$ The terms resistor performance mode and R-perf mode are used interchangeably.
${ }^{4}$ Guaranteed by design; not subject to production test.
${ }^{5}$ INL and DNL are measured at $V_{W}$ with the RDAC configured as a potentiometer divider similar to a voltage output $D A C . V_{A}=V_{D D}$ and $V_{B}=0$ V. DNL specification limits of $\pm 1$ LSB maximum are guaranteed monotonic operating conditions.
${ }^{6}$ The A, B, and W resistor terminals have no limitations on polarity with respect to each other. Dual-supply operation enables ground-referenced bipolar signal adjustment.
${ }^{7} P_{\text {DIISS }}$ is calculated from ( $\left.I_{\text {DD }} \times \mathrm{V}_{\text {DD }}\right)+\left(\mathrm{I}_{\text {SS }} \times \mathrm{V}_{\text {SS }}\right)+\left(I_{\text {LOGIC }} \times \mathrm{V}_{\text {LOGIC }}\right)$.
${ }^{8}$ All dynamic characteristics use $\mathrm{V}_{\mathrm{DD}}=+15 \mathrm{~V}, \mathrm{~V}_{S S}=-15 \mathrm{~V}$, and $\mathrm{V}_{\text {LOGIC }}=5 \mathrm{~V}$.

## RESISTOR PERFORMANCE MODE CODE RANGE—20 k』 VERSIONS

Table 2.

| Resistor Tolerance per Code | $\mathrm{R}_{\text {AB }}=20 \mathrm{k} \Omega$ |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\left\|\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\text {SS }}\right\|=30 \mathrm{~V}$ to 33 V |  | $\left\|\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{5 S}\right\|=26 \mathrm{~V}$ to $\mathbf{3 0} \mathrm{V}$ |  | $\left\|\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\text {SS }}\right\|=22 \mathrm{~V}$ to 26 V |  | $\left\|\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\text {Ss }}\right\|=21 \mathrm{~V}$ to 22 V |  |
|  | Rws | Rwa | Rwb | Rwa | Rwb | Rwa | Rws | Rwa |
| 1\% R-Tolerance | $\begin{aligned} & \text { From } 0 \times 15 \mathrm{E} \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | $\begin{aligned} & \text { From 0x000 } \\ & \text { to } 0 \times 2 \mathrm{~A} 1 \end{aligned}$ | $\begin{aligned} & \text { From 0x1F4 } \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 20 B \end{aligned}$ | $\begin{aligned} & \text { From 0x1F4 } \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | $\begin{aligned} & \text { From 0x000 } \\ & \text { to } 0 \times 20 \mathrm{~B} \end{aligned}$ | N/A | N/A |
| 2\% R-Tolerance | From 0x8C to $0 \times 3 F F$ | From 0x000 to $0 \times 373$ | From 0xB4 to $0 \times 3$ FF | From 0x000 to $0 \times 34 \mathrm{~B}$ | From 0xFA to $0 \times 3 F F$ | From 0x000 to $0 \times 305$ | From 0xFA to 0x3FF | From 0x000 to $0 \times 305$ |
| 3\% R-Tolerance | $\begin{aligned} & \text { From } 0 \times 5 \mathrm{~A} \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 3 \mathrm{~A} 5 \end{aligned}$ | From 0x64 to 0x3FF | $\begin{aligned} & \text { From 0x000 } \\ & \text { to } 0 \times 39 B \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 78 \\ & \text { to } 0 \times 3 F F \end{aligned}$ | From 0x000 to $0 \times 387$ | $\begin{aligned} & \text { From } 0 \times 78 \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | From 0x000 to $0 \times 387$ |

## ELECTRICAL CHARACTERISTICS— $\mathbf{5 0} \mathbf{~ k} \Omega$ AND $\mathbf{1 0 0} \mathbf{k} \boldsymbol{\Omega}$ VERSIONS

$\mathrm{V}_{\mathrm{DD}}=21 \mathrm{~V}$ to $33 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=0 \mathrm{~V} ; \mathrm{V}_{\mathrm{DD}}=10.5 \mathrm{~V}$ to $16.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=-10.5 \mathrm{~V}$ to $-16.5 \mathrm{~V} ; \mathrm{V}_{\text {LOGIC }}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{DD}}, \mathrm{V}_{\mathrm{B}}=\mathrm{V}_{\mathrm{SS}}$, $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+105^{\circ} \mathrm{C}$, unless otherwise noted.

Table 3.

| Parameter | Symbol | Conditions | Min | Typ ${ }^{1}$ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC CHARACTERISTICS, RHEOSTAT MODE |  |  |  |  |  |  |
| Resolution | $N$ |  | 10 |  |  | Bits |
| Resistor Differential Nonlinearity ${ }^{2}$ | R-DNL | Rwb | -1 |  | +1 | LSB |
| Resistor Integral Nonlinearity ${ }^{2}$ | R-INL |  | -2 |  | +2 | LSB |
| Nominal Resistor Tolerance (R-Perf Mode) ${ }^{3}$ | $\Delta \mathrm{RAB}^{\prime} / \mathrm{R}_{\text {AB }}$ | See Table 4 | -1 | $\pm 0.5$ | +1 |  |
| Nominal Resistor Tolerance (Normal Mode) | $\Delta R_{A B} / R_{A B}$ |  |  | $\pm 20$ |  | \% |
| Resistance Temperature Coefficient ${ }^{4}$ | $\left(\Delta \mathrm{R}_{A B} / \mathrm{R}_{\text {AB }}\right) / \Delta \mathrm{T} \times 10^{6}$ |  |  | 35 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| Wiper Resistance | Rw |  |  | 60 | 100 | $\Omega$ |
| DC CHARACTERISTICS, POTENTIOMETER DIVIDER MODE |  |  |  |  |  |  |
| Resolution | N |  | 10 |  |  | Bits |
| Differential Nonlinearity ${ }^{5}$ | DNL |  | -1 |  | +1 | LSB |
| Integral Nonlinearity ${ }^{5}$ | INL |  | -1.5 |  | +1.5 | LSB |
| Voltage Divider Temperature Coefficient ${ }^{4}$ | $\left(\Delta \mathrm{V}_{\mathrm{W}} / \mathrm{V}_{\mathrm{W}}\right) / \Delta \mathrm{T} \times 10^{6}$ | Code $=$ half scale |  | 5 |  | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Full-Scale Error | $V_{\text {wfSE }}$ | Code $=$ full scale | -8 |  | +1 | LSB |
| Zero-Scale Error | V wZSE | Code $=$ zero scale | 0 |  | 8 | LSB |
| RESISTOR TERMINALS |  |  |  |  |  |  |
| Terminal Voltage Range ${ }^{6}$ | $V_{A}, V_{B}, V_{W}$ |  | $\mathrm{V}_{\text {ss }}$ |  | $V_{D D}$ | V |
| Capacitance A, Capacitance B4 | $C_{\text {A }}, C_{B}$ | $\mathrm{f}=1 \mathrm{MHz}$, measured to GND, code $=$ half-scale |  | 85 |  | pF |
| Capacitance W ${ }^{4}$ | $\mathrm{C}_{\mathrm{w}}$ | $\mathrm{f}=1 \mathrm{MHz}$, measured to GND, code $=$ half-scale |  | 65 |  | pF |
| Common-Mode Leakage Current | Ісм | $\mathrm{V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{B}}=\mathrm{V}_{\mathrm{W}}$ |  | $\pm 1$ |  | nA |
| DIGITAL INPUTS |  |  | JEDE | C comp |  |  |
| Input Logic High | $\mathrm{V}_{\mathrm{IH}}$ | $\mathrm{V}_{\text {Logic }}=2.7 \mathrm{~V}$ to 5.5 V | 2.0 |  |  | V |
| Input Logic Low | $\mathrm{V}_{\text {IL }}$ | $\mathrm{V}_{\text {Logic }}=2.7 \mathrm{~V}$ to 5.5 V |  |  | 0.8 | V |
| Input Current | ILL | $\mathrm{V}_{\text {IN }}=0 \mathrm{~V}$ or $\mathrm{V}_{\text {Logic }}$ |  |  | $\pm 1$ | $\mu \mathrm{A}$ |
| Input Capacitance ${ }^{4}$ | $\mathrm{Cl}_{\text {IL }}$ |  |  | 5 |  | pF |
| DIGITAL OUTPUTS (SDO and RDY) |  |  |  |  |  |  |
| Output High Voltage | $\mathrm{V}_{\mathrm{OH}}$ | Reull_up $=2.2 \mathrm{k} \Omega$ to $\mathrm{V}_{\text {LOGIC }}$ | $\mathrm{V}_{\text {LOGIC }}-0.4$ |  |  | V |
| Output Low Voltage | Vol | RPULL_UP $=2.2 \mathrm{k} \Omega$ to $\mathrm{V}_{\text {LOGIC }}$ |  |  | GND+0.4 | V |
| Tristate Leakage Current |  |  | -1 |  | +1 | $\mu \mathrm{A}$ |
| Output Capacitance ${ }^{4}$ | Col |  |  | 5 |  | pF |
| POWER SUPPLIES |  |  |  |  |  |  |
| Single-Supply Power Range | $V_{\text {D }}$ | $\mathrm{V}_{\mathrm{ss}}=0 \mathrm{~V}$ | 9 |  | 33 | V |
| Dual-Supply Power Range | VDD/VSS |  | $\pm 9$ |  | $\pm 16.5$ | V |
| Positive Supply Current | ld | $\mathrm{V}_{\mathrm{DD}} / \mathrm{V}_{S S}= \pm 16.5 \mathrm{~V}$ |  | 0.1 | 2 | $\mu \mathrm{A}$ |
| Negative Supply Current | Iss | $\mathrm{V}_{\mathrm{DD}} / \mathrm{V}_{\mathrm{SS}}= \pm 16.5 \mathrm{~V}$ | -2 | -0.1 |  | $\mu \mathrm{A}$ |
| Logic Supply Range | $V_{\text {LOGIC }}$ |  | 2.7 |  | 5.5 | V |
| Logic Supply Current | ILogic | $\mathrm{V}_{\text {LoGIC }}=5 \mathrm{~V} ; \mathrm{V}_{\text {IH }}=5 \mathrm{~V}$ or $\mathrm{V}_{\text {IL }}=\mathrm{GND}$ |  | 1 | 10 | $\mu \mathrm{A}$ |
| Power Dissipation ${ }^{7}$ | PDISS | $\mathrm{V}_{\mathrm{HH}}=5 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{IL}}=\mathrm{GND}$ |  | 8 | 110 | $\mu \mathrm{W}$ |
| Power Supply Rejection Ratio ${ }^{4}$ | PSSR | $\Delta \mathrm{V}_{\text {DD }} / \Delta \mathrm{V}_{\text {SS }}= \pm 15 \mathrm{~V} \pm 10 \%$ |  |  |  |  |
|  |  | $\mathrm{R}_{A B}=50 \mathrm{k} \Omega$ |  | 0.039 |  | \%/\% |
|  |  | $\mathrm{R}_{\mathrm{AB}}=100 \mathrm{k} \Omega$ |  | 0.021 |  | \%/\% |


| Parameter | Symbol | Conditions | Min | Typ ${ }^{1}$ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DYNAMIC CHARACTERISTICS ${ }^{4,8}$ |  |  |  |  |  |  |
| Bandwidth | BW | -3 dB |  |  |  | kHz |
|  |  | $\mathrm{R}_{A B}=50 \mathrm{k} \Omega$ |  | 210 |  |  |
|  |  | $\mathrm{R}_{\text {AB }}=100 \mathrm{k} \Omega$ |  | 105 |  |  |
| Total Harmonic Distortion | THDw | $\mathrm{V}_{\mathrm{A}}=1 \mathrm{Vrms}, \mathrm{V}_{\mathrm{B}}=0 \mathrm{~V}, \mathrm{f}=1 \mathrm{kHz}$ |  |  |  |  |
|  |  | $\mathrm{R}_{\mathrm{AB}}=50 \mathrm{k} \Omega$ |  | -101 |  | dB |
|  |  | $\mathrm{R}_{\text {AB }}=100 \mathrm{k} \Omega$ |  | -106 |  | dB |
| Vw Settling Time | ts | $\begin{aligned} & \mathrm{V}_{\mathrm{A}}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{B}}=0 \mathrm{~V}, \pm 0.5 \mathrm{LSB} \text { error } \\ & \text { band, initial code }=\text { zero scale } \end{aligned}$ |  |  |  |  |
|  |  | Code $=$ full scale, R-normal mode |  | 750 |  | ns |
|  |  | Code $=$ full scale, R-perf mode |  | 2.5 |  | $\mu \mathrm{s}$ |
|  |  | $\begin{aligned} & \text { Code }=\text { half scale, } \mathrm{R} \text {-normal mode, } \\ & \mathrm{R}_{A B}=50 \mathrm{k} \Omega \end{aligned}$ |  | 7 |  | $\mu \mathrm{s}$ |
|  |  | $\begin{aligned} & \text { Code }=\text { half scale, } \mathrm{R} \text {-normal mode, } \\ & \mathrm{R}_{A B}=100 \mathrm{k} \Omega \end{aligned}$ |  | 14 |  | $\mu \mathrm{s}$ |
|  |  | $\begin{aligned} & \text { Code = half scale, } \mathrm{R} \text {-perf mode, } \\ & \mathrm{R}_{A B}=50 \mathrm{k} \Omega \end{aligned}$ |  | 9 |  | $\mu \mathrm{s}$ |
|  |  | $\begin{aligned} & \text { Code }=\text { half scale, } \mathrm{R} \text {-perf mode, } \\ & \mathrm{R}_{A B}=100 \mathrm{k} \Omega \end{aligned}$ |  | 16 |  | $\mu \mathrm{s}$ |
| Resistor Noise Density | $\mathrm{e}_{\text {N_wb }}$ | $\begin{aligned} & \text { Code }=\text { half scale, } \mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \\ & 0 \mathrm{kHz} \text { to } 200 \mathrm{kHz}, \end{aligned}$ |  |  |  |  |
|  |  | $\mathrm{R}_{A B}=50 \mathrm{k} \Omega$ |  | 18 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
|  |  | $\mathrm{R}_{\text {AB }}=100 \mathrm{k} \Omega$ |  | 27 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |

${ }^{1}$ Typicals represent average readings at $25^{\circ} \mathrm{C} ; \mathrm{V}_{\mathrm{DD}}=+15 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=-15 \mathrm{~V}$, and $\mathrm{V}_{\text {LOGIC }}=5 \mathrm{~V}$.
${ }^{2}$ Resistor position nonlinearity error. R-INL is the deviation from an ideal value measured between $\mathrm{R}_{\mathrm{w}}$ at Code $0 \times 00 \mathrm{~B}$ to Code $0 \times 3 \mathrm{FF}$ or between RwA at Code $0 \times 3 \mathrm{~F} 3$ to Code $0 \times 000$. R-DNL measures the relative step change from ideal between successive tap positions. The specification is guaranteed in resistor performance mode with a wiper current of 1 mA for $\mathrm{V}_{\mathrm{A}}<12 \mathrm{~V}$ and 1.2 mA for $\mathrm{V}_{\mathrm{A}} \geq 12 \mathrm{~V}$.
${ }^{3}$ The terms resistor performance mode and R-perf mode are used interchangeably.
${ }^{4}$ Guaranteed by design; not subject to production test.
${ }^{5}$ INL and DNL are measured at $V_{W}$ with the RDAC configured as a potentiometer divider similar to a voltage output $D A C . V_{A}=V_{D D}$ and $V_{B}=0$ V. DNL specification limits of $\pm 1$ LSB maximum are guaranteed monotonic operating conditions.
${ }^{6}$ The A, B, and W resistor terminals have no limitations on polarity with respect to each other. Dual-supply operation enables ground-referenced bipolar signal adjustment.
${ }^{7}$ PDIISS is calculated from ( $\left.I_{\text {DD }} \times \mathrm{V}_{\text {DD }}\right)+\left(\mathrm{I}_{\text {SS }} \times \mathrm{V}_{\text {SS }}\right)+$ (ILOGIC $\left.\times \mathrm{V}_{\text {LOGIC }}\right)$.
${ }^{8}$ All dynamic characteristics use $\mathrm{V}_{\mathrm{DD}}=+15 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=-15 \mathrm{~V}$, and $\mathrm{V}_{\mathrm{LOGIC}}=5 \mathrm{~V}$.

## RESISTOR PERFORMANCE MODE CODE RANGE—50 k AND 100 k $\Omega$ VERSIONS

Table 4.

| Resistor Tolerance per Code | $\mathrm{R}_{\text {AB }}=50 \mathrm{k} \Omega$ |  |  |  | $\mathrm{R}_{\mathrm{AB}}=100 \mathrm{k} \Omega$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\left\|V_{\text {DD }}-V_{S S}\right\|=26 \mathrm{~V}$ to 33 V |  | \| $\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\text {SS }} \mid=21 \mathrm{~V}$ to 26 V |  | $\left\|V_{\text {dD }}-V_{S S}\right\|=26 \mathrm{~V}$ to 33 V |  | $\left\|\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\text {Ss }}\right\|=21 \mathrm{~V}$ to 26 V |  |
|  | Rwb | Rwa | Rwi | Rwa | Rwb | Rwa | Rwb | Rwa |
| 1\% R-Tolerance | From 0x08C to $0 \times 3 F F$ | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 35 \mathrm{~F} \end{aligned}$ | From 0x0B4 to $0 \times 3$ FF | From 0x000 to $0 \times 31 \mathrm{E}$ | From 0x04B to $0 \times 3 F F$ | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 3 \mathrm{~B} 4 \end{aligned}$ | From 0x064 to $0 \times 3$ FF | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 39 \mathrm{~B} \end{aligned}$ |
| 2\% R-Tolerance | From 0X03C to $0 \times 3 F F$ | $\begin{aligned} & \text { From 0x000 } \\ & \text { to } 0 \times 3 \mathrm{C} 3 \end{aligned}$ | $\begin{aligned} & \text { From 0x050 } \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | From 0x000 to $0 \times 3 \mathrm{AF}$ | $\begin{aligned} & \text { From } 0 \times 028 \\ & \text { to } 0 \times 3 F F \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 3 D 7 \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 028 \\ & \text { to } 0 \times 3 F F \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 000 \\ & \text { to } 0 \times 3 D 7 \end{aligned}$ |
| 3\% R-Tolerance | From 0X028 to $0 \times 3 \mathrm{FF}$ | From 0x000 to 0x3D7 | $\begin{aligned} & \text { From 0x032 } \\ & \text { to } 0 \times 3 \mathrm{FF} \end{aligned}$ | From 0x000 to $0 \times 3 C D$ | $\text { From } 0 \times 019$ $\text { to } 0 \times 3 F F$ | $\begin{aligned} & \text { From 0x000 } \\ & \text { to } 0 \times 3 E 6 \end{aligned}$ | $\begin{aligned} & \text { From } 0 \times 019 \\ & \text { to } 0 \times 3 F F \end{aligned}$ | $\begin{aligned} & \text { From 0x000 } \\ & \text { to } 0 \times 3 E 6 \end{aligned}$ |

AD5293

## INTERFACE TIMING SPECIFICATIONS

$\mathrm{V}_{\mathrm{DD}}=\mathrm{V}_{\text {SS }}= \pm 15 \mathrm{~V}, \mathrm{~V}_{\text {LOGIC }}=2.7 \mathrm{~V}$ to 5.5 V , and $-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+105^{\circ} \mathrm{C}$. All specifications $\mathrm{T}_{\mathrm{MIN}}$ to $\mathrm{T}_{\mathrm{MAX}}$, unless otherwise noted.
Table 5.

| Parameter | Limit ${ }^{1}$ | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: |
| $\mathrm{t}_{1}{ }^{2}$ | 20 | ns min | SCLK cycle time |
| $\mathrm{t}_{2}$ | 10 | ns min | SCLK high time |
| $\mathrm{t}_{3}$ | 10 | ns min | SCLK low time |
| $\mathrm{t}_{4}$ | 10 | ns min | $\overline{\text { SYNC }}$ to SCLK falling edge setup time |
| $\mathrm{t}_{5}$ | 5 | ns min | Data setup time |
| $\mathrm{t}_{6}$ | 5 | ns min | Data hold time |
| $\mathrm{t}_{7}$ | 1 | ns min | SCLK falling edge to $\overline{S Y N C}$ rising edge |
| $\mathrm{t}_{8}$ | $400^{3}$ | ns min | Minimum $\overline{\text { SYNC }}$ high time |
| $\mathrm{t}_{9}$ | 14 | ns min | $\overline{\text { SYNC }}$ rising edge to next SCLK fall ignored |
| $\mathrm{t}_{10}{ }^{4}$ | 1 | ns min | RDY rise to $\overline{\text { SYNC }}$ falling edge |
| $\mathrm{t}_{11}{ }^{4}$ | 40 | ns max | $\overline{\text { SYNC }}$ rise to RDY fall time |
| $\mathrm{t}_{12}{ }^{4}$ | 2.4 | $\mu \mathrm{s}$ max | RDY low time, RDAC register write command execute time (resistor performance mode) |
| $\mathrm{t}_{12}{ }^{4}$ | 410 | ns max | RDY low time, RDAC register write command execute time (normal mode) |
| $\mathrm{t}_{12}{ }^{4}$ | 1.5 | ms max | Software\hardware reset |
| $\mathrm{t}_{13}{ }^{4}$ | 450 | ns max | RDY low time, RDAC register read command execute time |
| $\mathrm{t}_{14}{ }^{4}$ | 450 | ns max | SCLK rising edge to SDO valid |
| $\mathrm{t}_{\text {RESET }}$ | 20 | ns min | Minimum $\overline{\text { RESET }}$ pulse width (asynchronous) |
| tpower-up ${ }^{5}$ | 2 | ms max | Power-on time to half scale |

[^0]

Figure 2. Shift Register Contents

## TIMING DIAGRAMS



Figure 3. Write Timing Diagram, $C P O L=0, C P H A=1$


Figure 4. Read Timing Diagram, $C P O L=0, C P H A=1$

## ABSOLUTE MAXIMUM RATINGS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 6.

| Parameter | Rating |
| :---: | :---: |
| $V_{\text {DD }}$ to GND | -0.3 V to +35 V |
| Vss to GND | +0.3 V to -25 V |
| VLogic to GND | -0.3 V to +7 V |
| $V_{\text {DD }}$ to $V_{\text {Ss }}$ | 35 V |
| $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{B}}, \mathrm{V}_{\mathrm{w}}$ to GND | $\mathrm{V}_{\text {SS }}-0.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}+0.3 \mathrm{~V}$ |
| Digital Input and Output Voltage to GND | -0.3 V to $\mathrm{V}_{\text {Logic }}+0.3 \mathrm{~V}$ |
| EXT_CAP Voltage to GND | -0.3 V to +7 V |
| $\mathrm{I}_{\mathrm{A}}, \mathrm{I}_{\mathrm{B}}, \mathrm{I}_{\mathrm{w}}$ |  |
| Continuous |  |
| $\mathrm{R}_{A B}=20 \mathrm{k} \Omega$ | $\pm 3 \mathrm{~mA}$ |
| $\mathrm{R}_{\text {AB }}=50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ | $\pm 2 \mathrm{~mA}$ |
| Pulsed ${ }^{1}$ |  |
| Frequency $>10 \mathrm{kHz}$ | MCC ${ }^{2} / \mathrm{d}^{3}$ |
| Frequency $\leq 10 \mathrm{kHz}$ | $\mathrm{MCC}^{2} / \sqrt{ } \mathrm{d}^{3}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ |
| Maximum Junction Temperature ( $T$, max) | $150^{\circ} \mathrm{C}$ |
| Storage Temperature Range | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Reflow Soldering |  |
| Peak Temperature | $260^{\circ} \mathrm{C}$ |
| Time at Peak Temperature | 20 sec to 40 sec |
| Package Power Dissipation | $\left(\mathrm{T}, \max -\mathrm{T}_{\mathrm{A}}\right.$ ) $/ \theta_{\mathrm{JA}}$ |

${ }^{1}$ Maximum terminal current is bounded by the maximum current handling of the switches, maximum power dissipation of the package, and maximum applied voltage across any two of the $A, B$, and $W$ terminals at a given resistance.
${ }^{2}$ Maximum continuous current.
${ }^{3}$ Pulse duty factor.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{\text {IA }}$ is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages.

Table 7. Thermal Resistance

| Package Type | $\boldsymbol{\theta}_{\mathbf{J A}}$ | $\boldsymbol{\theta}_{\mathbf{J c}}$ | Unit |
| :--- | :--- | :--- | :--- |
| 14-Lead TSSOP | $93^{1}$ | 20 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Figure 5. Pin Configuration

Table 8. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | $\overline{\text { RESET }}$ | Hardware Reset Pin. Sets the RDAC register to midscale. $\overline{\text { RESET }}$ is activated at the logic high transition. Tie $\overline{\mathrm{RESET}}$ to $V_{\text {Logic }}$ if not used. |
| 2 | $\mathrm{V}_{\text {ss }}$ | Negative Supply. Connect to 0 V for single-supply applications. This pin should be decoupled with $0.1 \mu \mathrm{~F}$ ceramic capacitors and $10 \mu \mathrm{~F}$ capacitors. |
| 3 | A | Terminal A of RDAC. $\mathrm{V}_{S S} \leq \mathrm{V}_{\mathrm{A}} \leq \mathrm{V}_{\mathrm{DD}}$. |
| 4 | W | Wiper Terminal W of RDAC. $\mathrm{V}_{\text {SS }} \leq \mathrm{V}_{\mathrm{W}} \leq \mathrm{V}_{\mathrm{DD}}$. |
| 5 | B | Terminal B of RDAC. $\mathrm{V}_{S S} \leq \mathrm{V}_{\mathrm{B}} \leq \mathrm{V}_{\mathrm{DD}}$. |
| 6 | VDD | Positive Power Supply. This pin should be decoupled with $0.1 \mu \mathrm{~F}$ ceramic capacitors and $10 \mu \mathrm{~F}$ capacitors. |
| 7 | EXT_CAP | Connect a $1 \mu \mathrm{~F}$ capacitor to EXT_CAP. This capacitor must have a voltage rating of $\geq 7 \mathrm{~V}$. |
| 8 | $V_{\text {Logic }}$ | Logic Power Supply, 2.7 V to 5.5 V. This pin should be decoupled with $0.1 \mu \mathrm{~F}$ ceramic capacitors and $10 \mu \mathrm{~F}$ capacitors. |
| 9 | GND | Ground Pin, Logic Ground Reference. |
| 10 | DIN | Serial Data Input. This part has a 16-bit shift register. Data is clocked into the register on the falling edge of the serial clock input. |
| 11 | SCLK | Serial Clock Input. Data is clocked into the shift register on the falling edge of the serial clock input. Data can be transferred at rates up to 50 MHz . |
| 12 | $\overline{\text { SYNC }}$ | Falling Edge Synchronization Signal. This is the frame synchronization signal for the input data. When $\overline{\text { SYNC }}$ goes low, it enables the shift register, and data is transferred in on the falling edges of the following clocks. The selected register is updated on the rising edge of $\overline{\text { SYNC }}$, following the $16^{\text {th }}$ clock cycle. If $\overline{\text { SYNC }}$ is taken high before the $16^{\text {th }}$ clock cycle, the rising edge of $\overline{\text { SYNC }}$ acts as an interrupt, and the write sequence is ignored by the DAC. |
| 13 | SDO | Serial Data Output. This open-drain output requires an external pull-up resistor. SDO can be used to clock data from the serial register in daisy-chain mode or in readback mode. |
| 14 | RDY | Ready Pin. This active-high, open-drain output identifies the completion of a write or read operation to or from the RDAC register. |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 6. $R$-INL in R-Perf Mode vs. Code vs. Temperature


Figure 7. R-DNL in R-Perf Mode vs. Code vs. Temperature


Figure 8. R-INL in Normal Mode vs. Code vs. Temperature


Figure 9. R-INL in R-Perf Mode vs. Code vs. Nominal Resistance


Figure 10. R-DNL in R-Perf Mode vs. Code vs. Nominal Resistance


Figure 11. R-INL in Normal Mode vs. Code vs. Nominal Resistance


Figure 12. R-DNL in Normal Mode vs. Code vs. Temperature


Figure 13. INL in R-Perf Mode vs. Code vs. Temperature


Figure 14. DNL in R-Perf Mode vs. Code vs. Temperature


Figure 15. R-DNL in Normal Mode vs. Code vs. Nominal Resistance


Figure 16. INL in R-Perf Mode vs. Code vs. Nominal Resistance


Figure 17. DNL in R-Perf Mode vs. Code vs. Nominal Resistance


Figure 18. INL in Normal Mode vs. Code vs. Temperature


Figure 19. DNL in Normal Mode vs. Code vs. Temperature


Figure 20. Supply Current vs. Temperature


Figure 21. INL in Normal Mode vs. Code vs. Nominal Resistance


Figure 22. DNL in Normal Mode vs. Code vs. Nominal Resistance


Figure 23. Supply Current, LLOGI, vs. Digital Input Voltage.


Figure 24. Rheostat Mode Tempco $\Delta R W B / \Delta T$ vs. Code


Figure 25. $20 \mathrm{k} \Omega$ Gain vs. Frequency vs. Code


Figure $26.50 \mathrm{k} \Omega$ Gain vs. Frequency vs. Code


Figure 27. Potentiometer Mode Tempco $\triangle R W B / \Delta T$ vs. Code


Figure $28.100 \mathrm{k} \Omega$ Gain vs. Frequency vs. Code


Figure 29. Power Supply Rejection Ratio (PSRR) vs. Frequency


Figure 30. Total Harmonic Distortion + Noise $(T H D+N)$ vs. Frequency


Figure 31. Maximum Bandwidth vs. Code vs. Net Capacitance


Figure 32. Large Signal Settling Time, Code from Zero Scale to Full Scale


Figure 33. Total Harmonic Distortion + Noise $(T H D+N)$ vs. Amplitude


Figure 34. Theoretical Maximum Current vs. Code


Figure 35. Digital Feedthrough


Figure 36. Maximum Transition Glitch


Figure 37. Code Range > 1\% R-Tolerance Error vs. Temperature


Figure 38. Code Range > $1 \%$ R-Tolerance Error vs. Voltage

TEST CIRCUITS
Figure 39 to Figure 44 define the test conditions used in the Specifications section.


Figure 39. Resistor Position Nonlinearity Error (Rheostat Operation: R-INL, R-DNL)


Figure 40. Potentiometer Divider Nonlinearity Error (INL, DNL)


Figure 41. Wiper Resistance


Figure 42. Power Supply Sensitivity (PSS, PSRR)


Figure 43. Gain vs. Frequency


Figure 44. Common-Mode Leakage Current

## THEORY OF OPERATION

The AD5293 digital potentiometer is designed to operate as a true variable resistor for analog signals that remain within the terminal voltage range of $\mathrm{V}_{\text {SS }}<\mathrm{V}_{\text {TERM }}<\mathrm{V}_{\mathrm{DD}}$. The patented $\pm 1 \%$ resistor tolerance feature helps to minimize the total RDAC resistance error, which reduces the overall system error by offering better absolute matching and improved open-loop performance. The digital potentiometer wiper position is determined by the RDAC register contents. The RDAC register acts as a scratchpad register, allowing as many value changes as necessary to place the potentiometer wiper in the correct position. The RDAC register can be programmed with any position setting via the standard serial peripheral interface (SPI) by loading the 16 -bit data-word.

## SERIAL DATA INTERFACE

The AD5293 contains a serial interface ( $\overline{\text { SYNC }}$, SCLK, DIN, and SDO) that is compatible with SPI standards, as well as most DSPs. The device allows data to be written to every register via the SPI.

## SHIFT REGISTER

The AD5293 shift register is 16 bits wide (see Figure 2). The 16-bit data-word consists of two unused bits, which are set to 0 , followed by four control bits and 10 RDAC data bits. Data is loaded MSB first (Bit 15). The four control bits determine the function of the software command (see Table 11). Figure 3 shows a timing diagram of a typical write sequence.
The write sequence begins by bringing the $\overline{S Y N C}$ line low. The $\overline{\text { SYNC }}$ pin must be held low until the complete data-word is loaded from the DIN pin. When $\overline{\text { SYNC }}$ returns high, the serial data-word is decoded according to the instructions in Table 11. The command bits ( Cx ) control the operation of the digital potentiometer. The data bits ( Dx ) are the values that are loaded into the decoded register. The AD5293 has an internal counter that counts a multiple of 16 bits (per frame) for proper operation. For example, the AD5293 works with a 32 -bit word, but it cannot work properly with a 31- or 33-bit word. The AD5293 does not require a continuous SCLK, when $\overline{S Y N C}$ is high, and all interface pins should be operated close to the supply rails to minimize power consumption in the digital input buffers.

## RDAC REGISTER

The RDAC register directly controls the position of the digital potentiometer wiper. For example, when the RDAC register is loaded with all zeros, the wiper is connected to Terminal B of the variable resistor. The RDAC register is a standard logic register; there is no restriction on the number of changes allowed. The RDY pin can be used to monitor the completion of a write to or read from the RDAC register. The AD5293 presets to midscale on power-up.

## WRITE PROTECTION

On power-up, the serial data input register write command for the RDAC register is disabled. The RDAC write protect bit, C 1 of the control register (see Table 12 and Table 13), is set to 0 by default. This disables any change of the RDAC register content, regardless of the software commands, except that the RDAC register can be refreshed to midscale using the software reset command (Command 3, see Table 11) or through hardware, using the $\overline{\mathrm{RESET}}$ pin. To enable programming of the variable resistor wiper position (programming the RDAC register), the write protect bit, C 1 of the control register, must first be programmed. This is accomplished by loading the serial data input register with Command 4 (see Table 11).

## BASIC OPERATION

The basic mode of setting the variable resistor wiper position (programming the RDAC register) is accomplished by loading the serial data input register with Command 1 (see Table 11) and the desired wiper position data. The RDY pin can be used to monitor the completion of this RDAC register write command. Command 2 can be used to read back the contents of the RDAC register (see Table 11). After issuing the readback command, the RDY pin can be monitored to indicate when the data is available to be read out on SDO in the next SPI operation. Instead of monitoring the RDY pin, a minimum delay can be implemented when executing a write or read command (see Table 5). Table 9 provides an example listing of a sequence of serial data input (DIN) words with the serial data output appearing at the SDO pin in hexadecimal format for an RDAC write and read.

Table 9. RDAC Register Write and Read

| DIN | SDO | Action |
| :--- | :--- | :--- |
| $0 \times 1802$ | $0 \times$ XXXX $^{1}$ | Enable update of wiper position. |
| $0 \times 0500$ | $0 \times 1802$ | Write 0x100 to the RDAC register. <br> Wiper moves to $1 / 4$ <br> full-scale position. |
| $0 \times 0800$ | $0 \times 0500$ | Prepare data read from RDAC register. <br> $0 \times 0000$ |
| $0 \times 0100$ | NOP (Instruction 0) sends a 16-bit word <br> out of SDO, where the last 10 bits contain <br> the contents of the RDAC register. |  |

${ }^{1} \mathrm{X}=$ unknown.

## SHUTDOWN MODE

The AD5293 can be placed in shutdown mode by executing the software shutdown command (see Command 6 in Table 11), and setting the LSB to 1 . This feature places the RDAC in a special state in which Terminal A is open-circuited and Wiper W is connected to Terminal B. The contents of the RDAC register are unchanged by entering shutdown mode. However, all commands listed in Table 11 are supported while in shutdown mode.

## RESET

A low-to-high transition of the hardware RESET pin loads the RDAC register with midscale. The AD5293 can also be reset through software by executing Command 3 (see Table 11). The control register is restored with default bits (see Table 13).

## RESISTOR PERFORMANCE MODE

This mode activates a new, patented $1 \%$ end-to-end resistor tolerance that ensures a $\pm 1 \%$ resistor tolerance on each code, that is, code $=$ half scale, $\mathrm{R}_{\mathrm{WB}}=10 \mathrm{k} \Omega \pm 100 \Omega$. See Table 2 and Table 4 to verify which codes achieve $\pm 1 \%$ resistor tolerance. The resistor performance mode is activated by programming Bit C2 of the control register (see Table 12 and Table 13). The typical settling time is shown in Figure 32.

## SDO PIN AND DAISY-CHAIN OPERATION

The serial data output pin (SDO) serves two purposes: it can be used to read the contents of the wiper setting and control register using Command 2, and Command 5, respectively (see Table 11) or the SDO pin can be used in daisy-chain mode. Data is clocked out of SDO on the rising edge of SCLK. The SDO pin contains an open-drain N-channel FET that requires a pull-up resistor if this pin is used. To place the pin in high impedance and minimize the power dissipation when the pin is used, the $0 \times 8001$ data word followed by Command 0 should be sent to the part. Table 10 provides a sample listing for the
sequence of the serial data input (DIN). Daisy chaining minimizes the number of port pins required from the controlling IC. As shown in Figure 45, users need to tie the SDO pin of one package to the DIN pin of the next package. Users may need to increase the clock period, because the pull-up resistor and the capacitive loading at the SDO-to-DIN interface may require additional time delay between subsequent devices.

When two AD5293s are daisy-chained, 32 bits of data are required. The first 16 bits go to U 2 , and the second 16 bits go to U 1 . The $\overline{\text { SYNC }}$ pin should be held low until all 32 bits are clocked into their respective serial registers. The $\overline{\mathrm{SYNC}}$ pin is then pulled high to complete the operation.
Keep the $\overline{\text { SYNC }}$ pin low until all 32 bits are clocked into their respective serial registers. The $\overline{\mathrm{SYNC}} \mathrm{pin}$ is then pulled high to complete the operation.


Figure 45. Daisy-Chain Configuration Using SDO

Table 10. Minimize Power Dissipation at the SDO Pin

| DIN | SDO $^{1}$ | Action |
| :--- | :--- | :--- |
| $0 \times X X X X$ | $0 \times X X X X$ | Last user command sent to the digital potentiometer |
| $0 \times 8001$ | $0 \times X X X X$ | Prepares the SDO pin to be placed in high impedance mode |
| $0 \times 0000$ | High impedance | The SDO pin is placed in high impedance |
| ${ }^{1} \mathrm{X}=$ don't care. |  |  |

Table 11. Command Operation Truth Table

| Command | Command Bits[B13:B10] |  |  |  | Data Bits[B9:B0] ${ }^{1}$ |  |  |  |  |  |  |  |  |  | Operation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | C3 | C2 | C1 | C0 | D9 | D8 | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |  |
| 0 | 0 | 0 | 0 | 0 | X | X | X | X | X | X | X | X | X | X | NOP command. Do nothing. |
| 1 | 0 | 0 | 0 | 1 | D9 | D8 | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 | Write contents of serial register data to RDAC. |
| 2 | 0 | 0 | 1 | 0 | X | X | X | X | X | X | X | X | X | X | Read RDAC wiper setting from SDO output in the next frame. |
| 3 | 0 | 1 | 0 | 0 | X | X | X | X | X | X | X | X | X | X | Reset. Refresh RDAC with midscale code. |
| 4 | 0 | 1 | 1 | 0 | X | X | X | X | X | X | X | D2 | D1 | X | Write contents of serial register data to control register. |
| 5 | 0 | 1 | 1 | 1 | X | X | X | X | X | X | X | X | X | X | Read control register from SDO output in the next frame. |
| 6 | 1 | 0 | 0 | 0 | X | X | X | X | X | X | X | X | X | D0 | Software power-down. D0 $=0$ (normal mode). D0 $=1$ (device placed in shutdown mode). |

Table 12. Control Register Bit Map

| D9 | D8 | D7 | D6 | D5 | D4 | D3 | D2 | D1 | D0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | $\mathrm{X}^{1}$ | C 2 | $\mathrm{C}^{1}$ | $\mathrm{X}^{1}$ |

Table 13. Control Register Function

| Register Name | Bit Name | Description |
| :--- | :--- | :--- |
| Control | C2 | Calibration enable. |
|  |  | $0=$ resistor performance mode (default). |
|  |  | $1=$ normal mode. |
|  | C1 | RDAC register write protect. |
|  |  | $0=$ locks the wiper position through the digital interface (default). |
|  | $1=$ allows update of wiper position through digital interface. |  |

## RDAC ARCHITECTURE

To achieve optimum performance, Analog Devices, Inc., has patented the RDAC segmentation architecture for all the digital potentiometers. In particular, the AD5293 employs a 3-stage segmentation approach, as shown in Figure 46. The AD5293 wiper switch is designed with transmission gate CMOS topology and with the gate voltage derived from $V_{\text {DD }}$.


Figure 46. Simplified RDAC Circuit

## PROGRAMMING THE VARIABLE RESISTOR

## Rheostat Operation-1\% Resistor Tolerance

The AD5293 operates in rheostat mode when only two terminals are used as a variable resistor. The unused terminal can be left floating or it can be tied to the W terminal, as shown in Figure 47.


Figure 47. Rheostat Mode Configuration

The nominal resistance between Terminal A and Terminal B, $\mathrm{R}_{A B}$, is available in $20 \mathrm{k} \Omega, 50 \mathrm{k} \Omega$, and $100 \mathrm{k} \Omega$ and has 1024 tap points that are accessed by the wiper terminal. The 10-bit data in the RDAC latch is decoded to select one of the 1024 possible wiper settings. The AD5293 contains an internal $\pm 1 \%$ resistor tolerance calibration feature that can be enabled or disabled, enabled by default by programming Bit C2 of the control register (see Table 12 and Table 13).

The digitally programmed output resistance between the W terminal and the A terminal, $\mathrm{R}_{\mathrm{WA}}$, and the W terminal and B terminal, $\mathrm{R}_{\mathrm{wb}}$, is calibrated to give a maximum of $\pm 1 \%$ absolute resistance error over both the full supply and temperature ranges. As a result, the general equation for determining the digitally programmed output resistance between the W terminal and B terminal is

$$
\begin{equation*}
R_{W B}(D)=\frac{D}{1024} \times R_{A B} \tag{1}
\end{equation*}
$$

where:
$D$ is the decimal equivalent of the binary code loaded in the 10-bit RDAC register.
$R_{A B}$ is the end-to-end resistance.
Similar to the mechanical potentiometer, the resistance of the RDAC between the W terminal and the A terminal also produces a digitally controlled complementary resistance, $\mathrm{R}_{\mathrm{WA}}$. $\mathrm{R}_{\mathrm{WA}}$ is also calibrated to give a maximum of $1 \%$ absolute resistance error. $\mathrm{R}_{\mathrm{WA}}$ starts at the maximum resistance value and decreases as the data loaded into the latch increases. The general equation for this operation is

$$
\begin{equation*}
R_{W A}(D)=\frac{1024-D}{1024} \times R_{A B} \tag{2}
\end{equation*}
$$

where:
$D$ is the decimal equivalent of the binary code loaded in the 10-bit RDAC register.
$R_{A B}$ is the end-to-end resistance.
In the zero-scale condition, a finite total wiper resistance of $120 \Omega$ is present. Regardless of the setting in which the part is operating, care should be taken to limit the current between the A terminal to B terminal, the W terminal to the A terminal, and the W terminal to the B terminal to the maximum continuous current of $\pm 3 \mathrm{~mA}$ or to the pulse current specified in Table 6. Otherwise, degradation, or possible destruction of the internal switch contact, can occur.

## PROGRAMMING THE POTENTIOMETER DIVIDER

## Voltage Output Operation

The digital potentiometer easily generates a voltage divider at wiper-to-B terminal and wiper-to-A terminal that is proportional to the input voltage at $A$ to $B$, as shown in Figure 48. Unlike the polarity of $V_{D D}$ to GND, which must be positive, voltage across A to $\mathrm{B}, \mathrm{W}$ to A , and W to B can be at either polarity.


Figure 48. Potentiometer Mode Configuration
If ignoring the effect of the wiper resistance for simplicity, connecting the A terminal to 30 V and the B terminal to ground produces an output voltage at the Wiper W to Terminal B that ranges from 0 V to $30 \mathrm{~V}-1 \mathrm{LSB}$. Each LSB of voltage is equal to the voltage applied across the A terminal and B terminal, divided by the 1024 positions of the potentiometer divider. The general equation defining the output voltage at $\mathrm{V}_{\mathrm{W}}$, with respect to ground for any valid input voltage applied to Terminal A and Terminal B, is

$$
\begin{equation*}
V_{W}(D)=\frac{D}{1024} \times V_{A}+\frac{1024-D}{1024} \times V_{B} \tag{3}
\end{equation*}
$$

To optimize the wiper position update rate when in voltage divider mode, it is recommended that the internal $\pm 1 \%$ resistor tolerance calibration feature be disabled by programming Bit C2 of the control register (see Table 11).
Operation of the digital potentiometer in the divider mode results in a more accurate operation over temperature. Unlike rheostat mode, the output voltage is dependent mainly on the ratio of the internal resistors, $\mathrm{R}_{\mathrm{WA}}$ and $\mathrm{R}_{\mathrm{WB}}$, and not on the absolute values. Therefore, the temperature drift reduces to $5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.

## EXT_CAP CAPACITOR

A $1 \mu \mathrm{~F}$ capacitor to GND must be connected to the EXT_CAP pin (see Figure 49) on power-up and throughout the operation of the AD5293. This capacitor must have a voltage rating of $\geq 7 \mathrm{~V}$.


Figure 49. Hardware Setup for the EXT_CAP Pin

## TERMINAL VOLTAGE OPERATING RANGE

The positive $V_{D D}$ and negative $V_{\text {ss }}$ power supplies of the AD5293 define the boundary conditions for proper 3-terminal, digital potentiometer operation. Supply signals present on the A, B, and W terminals that exceed $\mathrm{V}_{\mathrm{DD}}$ or $\mathrm{V}_{\mathrm{SS}}$ are clamped by the internal forward-biased diodes (see Figure 50).


Figure 50. Maximum Terminal Voltages Set by $V_{D D}$ and $V_{S S}$
The ground pin of the AD5293 is primarily used as a digital ground reference. To minimize the digital ground bounce, the AD5293 ground pin should be joined remotely to common ground. The digital input control signals to the AD5293 must be referenced to the device ground pin (GND) to satisfy the logic level defined in the Specifications section.

## Power-Up Sequence

Because there are diodes to limit the voltage compliance at the A, B, and W terminals (see Figure 50), it is important to power $\mathrm{V}_{\mathrm{DD}}$ and $\mathrm{V}_{\mathrm{SS}}$ first, before applying any voltage to the $\mathrm{A}, \mathrm{B}$, and W terminals. Otherwise, the diode is forward-biased such that $V_{D D}$ and $V_{\text {ss }}$ are powered up unintentionally. The ideal power-up sequence is $G N D, V_{s s}, V_{\text {LOGIC }}, V_{D D}$, the digital inputs, and then $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{B}}$, and $\mathrm{V}_{\mathrm{w}}$. The order of powering up $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{B}}, \mathrm{V}_{\mathrm{W}}$, and the digital inputs is not important, as long as they are powered after $\mathrm{V}_{\mathrm{DD}}, \mathrm{V}_{\mathrm{SS}}$, and $\mathrm{V}_{\text {Logic. }}$
Regardless of the power-up sequence and the ramp rates of the power supplies, the power-on preset activates after $V_{\text {LOGIC }}$ is powered, restoring midscale to the RDAC register.

## APPLICATIONS INFORMATION

## HIGH VOLTAGE DAC

The AD5293 can be configured as a high voltage DAC, with an output voltage as high as 33 V . The circuit is shown in Figure 51. The output is

$$
\begin{equation*}
V_{\text {OUT }}(D)=\frac{D}{1024} \times\left[1.2 \mathrm{~V} \times\left(1+\frac{R_{2}}{R_{1}}\right)\right] \tag{4}
\end{equation*}
$$

where $D$ is the decimal code from 0 to 1023 .


Figure 51. High Voltage DAC

## PROGRAMMABLE VOLTAGE SOURCE WITH BOOSTED OUTPUT

For applications that require high current adjustments, such as a laser diode or tunable laser, a boosted voltage source can be considered (see Figure 52).


Figure 52. Programmable Boosted Voltage Source
In this circuit, the inverting input of the op amp forces $V_{\text {out }}$ to be equal to the wiper voltage set by the digital potentiometer. The load current is then delivered by the supply via the N-channel FET (U3). The N-channel FET power handling must be adequate to dissipate $\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {Out }}\right) \times \mathrm{I}_{\mathrm{L}}$ power. This circuit can source a maximum of 100 mA with a 33 V supply.

## HIGH ACCURACY DAC

It is possible to configure the AD5293 as a high accuracy DAC by optimizing the resolution of the device over a specific reduced voltage range. This is achieved by placing external resistors on either side of the RDAC, as shown in Figure 53. The improved $\pm 1 \%$ resistor tolerance specification greatly reduces error associated with matching to discrete resistors.

$$
\begin{equation*}
V_{\text {OUT }}(D)=\frac{R_{3}+\left(D / 1024 \times R_{A B}\right) \times V_{D D}}{R_{1}+\left({ }^{(1024-D) / 1024}\right) \times R_{A B}+R_{3}} \tag{5}
\end{equation*}
$$



Figure 53. Optimizing Resolution

## VARIABLE GAIN INSTRUMENTATION AMPLIFIER

The AD8221 in conjunction with the AD5293 and the ADG1207, as shown in Figure 54, make an excellent instrumentation amplifier for use in data acquisition systems. The data acquisition system is low distortion and low noise enable it to condition signals in front of a variety of ADCs.


Figure 54. Data Acquisition System
The gain can be calculated by using Equation 6, as follows:

$$
\begin{equation*}
G(D)=1+\frac{49.4 \mathrm{k} \Omega}{(D / 1024) \times R_{A B}} \tag{6}
\end{equation*}
$$

## AUDIO VOLUME CONTROL

The excellent THD performance and high voltage capability of the AD5293 make it ideal for digital volume control. The AD5293 is used as an audio attenuator; it can be connected directly to a gain amplifier. A large step change in the volume level at any arbitrary time can lead to an abrupt discontinuity of the audio signal, causing an audible zipper noise. To prevent this, a zero-crossing window detector can be inserted to the $\overline{\mathrm{CS}}$ line to delay the device update until the audio signal crosses the window. Because the input signal can operate on top of any dc level, rather than absolute 0 V level, zero crossing in this case means the signal is ac-coupled, and the dc offset level is the signal zero reference point.
The configuration to reduce zipper noise is shown in Figure 56, and the results of using this configuration are shown in Figure 55.

The input is ac-coupled by C 1 and attenuated down before feeding into the window comparator formed by $\mathrm{U} 2, \mathrm{U} 3$, and U 4 B . U6 is used to establish the signal as zero reference. The upper limit of the comparator is set above its offset and, therefore, the output pulses high whenever the input falls between 2.502 V and 2.497 V (or 0.005 V window) in this example. This output is AND'ed with the chip select signal such that the AD5293 updates whenever the signal crosses the window. To avoid a constant update of the device, program the chip select signal as two pulses instead of one.

In Figure 55, the lower trace shows that the volume level changes from a quarter-scale to full-scale when a signal change occurs near the zero-crossing window.


Figure 55. Zipper Noise Detector


Figure 56. Audio Volume Control with Zipper Noise Reduction.

## OUTLINE DIMENSIONS



Figure 57. 14-Lead Thin Shrink Small Outline Package [TSSOP]
(RU-14)
Dimensions shown in millimeters

## ORDERING GUIDE

| Model ${ }^{1}$ | R $\mathrm{AB}^{\text {( }} \mathrm{k}$ ) ) | Resolution | Temperature Range | Package Description | Package Option |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AD5293BRUZ-20 | 20 | 1024 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |
| AD5293BRUZ-20-RL7 | 20 | 1024 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |
| AD5293BRUZ-50 | 50 | 1024 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |
| AD5293BRUZ-50-RL7 | 50 | 1024 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |
| AD5293BRUZ-100 | 100 | 1024 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |
| AD5293BRUZ-100-RL7 | 100 | 1024 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 14-Lead TSSOP | RU-14 |

${ }^{1} \mathrm{Z}=$ RoHS Compliant Part.

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## http://moschip.ru/get-element

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Система менеджмента качества компании отвечает требованиям в соответствии с ГОСТ Р ИСО 9001, ГОСТ РВ 0015-002 и ЭС РД 009

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[^0]:    ${ }^{1}$ All input signals are specified with $\mathrm{t}_{\mathrm{R}}=\mathrm{t}_{\mathrm{F}}=1 \mathrm{~ns} / \mathrm{V}\left(10 \%\right.$ to $90 \%$ of $\left.\mathrm{V}_{\mathrm{DD}}\right)$ and timed from a voltage level of $\left(\mathrm{V}_{I L}+\mathrm{V}_{\mid H}\right) / 2$.
    ${ }^{2}$ Maximum SCLK frequency $=50 \mathrm{MHz}$.
    ${ }^{3}$ Refer to $t_{12}$ and $t_{13}$ for RDAC register commands operations.
    ${ }^{4}$ Rpull_up $=2.2 \mathrm{k} \Omega$ to V Logic with a capacitance load of 168 pF .
    ${ }^{5}$ Typical power supply voltage slew-rate of $2 \mathrm{~V} / \mathrm{ms}$.

