MP7748

2x20W Stereo Single Ended Class D Audio Amplifier

The Future of Analog IC Technology

DESCRIPTION

The MP7748 is a Class D Audio Amplifier for driving stereo speakers in single-ended configuration or a mono speaker in bridge-tied-load configuration. It is fully integrated audio amplifier which dramatically reduces solution size by integrating the following:

- 250mΩ power MOSFETs
- Startup / Shutdown pop elimination
- Short circuit protection circuits

The MP7748 is capable of delivering 20W per channel into 4Ω speaker in single-ended output structure, or delivering 50W into 6Ω speaker in bridge-tied-load output structure under 24V VDD. MPS Class D Audio Amplifiers exhibit the high fidelity of a Class A/B amplifier at high efficiencies. The circuit is based on the MPS' proprietary variable frequency topology that delivers excellent linearity, fast response time and operates on a single power supply.

MP7748 features programmable VDD shutdown voltage for each channel by controlling the UVP node voltage. The default VDD shutdown (rising threshold) voltage is 8.4V if the UVP pin is NC.

FEATURES

- Output Power at 24V VDD and 10% THD+N
  - Stereo SE configuration: 20W per channel into 4Ω load
  - Mono BTL configuration: 50W into 6Ω load
- THD+N = 0.02% at 1W, 8Ω(SE)
- Low Noise (103μV with SE configuration, 140μV with BTL configuration)
- Switching Frequency Up to 1MHz
- 9.5V to 36V Operation from a Single Supply
- Integrated Startup and Shutdown Pop Elimination Circuit
- Programmable UVP
- Thermal and Short Circuit Protection
- Integrated Power FETs
- Available in TSSOP28-Exposed Package

APPLICATIONS

- Portable Docking Stations
- Surround Sound DVD Systems
- Televisions
- Flat Panel Monitors
- Multimedia Computers
- Home Stereo Systems

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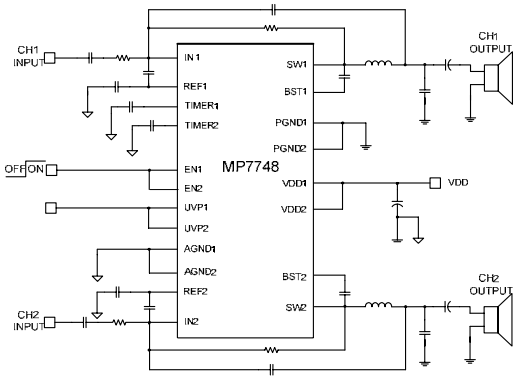
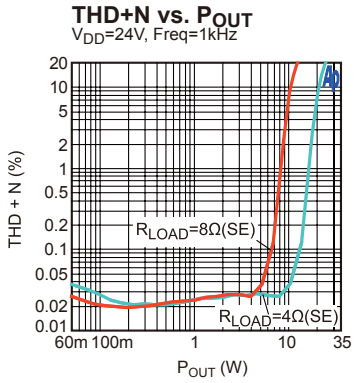
AAM (Analog Adaptive Modulation) is a Trademark of Monolithic Power Systems, Inc.

TYPICAL APPLICATION





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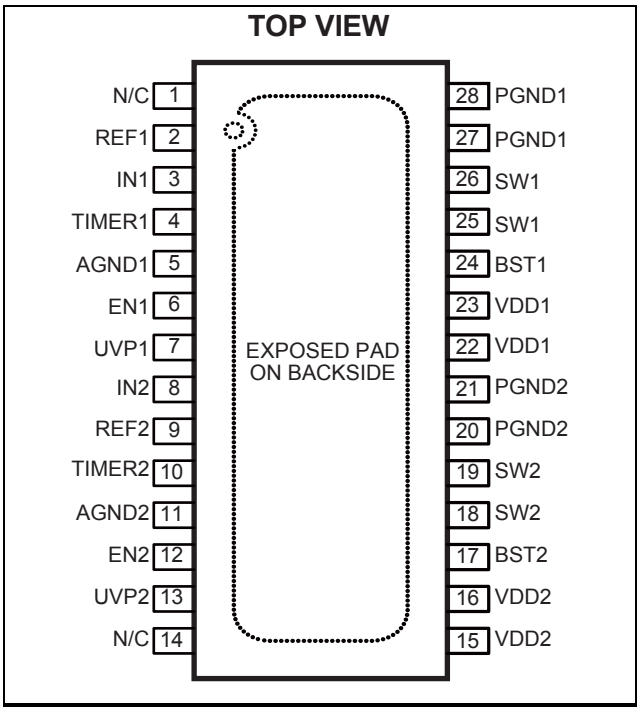
ORDERING INFORMATION

Part Number*	Package	Top Marking	Free Air Temperature (T_A)
MP7748DF	TSSOP28F	MP7748DF	-40°C to +85°C

* For Tape & Reel, add suffix –Z (e.g. MP7748DF–Z).
For RoHS compliant packaging, add suffix –LF (e.g. MP7748DF–LF–Z)

PACKAGE REFERENCE



ABSOLUTE MAXIMUM RATINGS (1)

Supply Voltage V_{DD} 40V
BS Voltage ..... V_{SW} – 0.3V to V_{SW} + 6.5V
Enable Voltage V_{EN} ..... -0.3V to +6V
V_{UVP}, V_{SW}, V_{PIN}, V_{NIN} ..... -1V to V_{DD} + 1V
AGND to PGND ..... -0.3V to +0.3V
Continuous Power Dissipation (T_A = +25°C) (2)
..... 3.9W
Junction Temperature ..... 150°C
Lead Temperature ..... 260°C
Storage Temperature ..... -65°C to +150°C

Recommended Operating Conditions (3)

Supply Voltage V_{DD} ..... 9.5V to 36V
Maximum Junction Temp. (T_J) ..... +125°C

Thermal Resistance (4)

	θ_{JA}	θ_{JC}	
TSSOP28F	32	6	°C

Notes:

1) Exceeding these ratings may damage the device.
2) The maximum allowable power dissipation is a function of the maximum junction temperature T_J (MAX), the junction-to-ambient thermal resistance θ_{JA}, and the ambient temperature T_A. The maximum allowable continuous power dissipation at any ambient temperature is calculated by PD (MAX) = (T_J(MAX)-T_A)/ θ_{JA}. Exceeding the maximum allowable power dissipation will cause excessive die temperature, and the regulator will go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
3) The device is not guaranteed to function outside of its operating conditions.
4) Measured on JESD51-7, 4-layer PCB.

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ELECTRICAL CHARACTERISTICS (5, 6)

V_{DD} = 24V, V_{EN} = 5V, T_A = +25°C, unless otherwise noted.

Parameters	Symbol	Condition	Min	Typ	Max	Units
Supply Current						
Standby Current		V_{EN} = 0V,NIN=PIN=Float		140		μA
Quiescent Current	I_Q	SW=Low		3	6	mA
Output Drivers						
SW On Resistance		Sourcing and Sinking		0.25		Ω
Short Circuit Current		Sourcing and Sinking		4.5		A
Inputs						
EN Enable Threshold Voltage		V_{EN} Rising		1.4	2.0	V
		V_{EN} Falling	0.4	1.0		V
EN Enable Input Current		V_{EN} = 5V		5		μA
External Undervoltage Detection	V_{UVP}			4		V
External Undervoltage Detection Hysteresis Voltage	V_{Hys}			0.3		V
Thermal Shutdown						
Thermal Shutdown Trip Point		T_J Rising		150		°C
Thermal Shutdown Hysteresis				30		°C

Note:

5) The device is not guaranteed to function outside its operating rating.
6) Electrical Characteristics are for the IC only with no external components except bypass capacitors.

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OPERATING SPECIFICATIONS

Circuit of figure 5, single-ended output configuration, V_{DD} = 24V, Gain=8.25V/V, V_{EN} = 5V, T_A = +25°C, unless otherwise noted.

Parameters	Symbol	Condition		Min	Typ	Max	Units
Standby Current		V_{EN} = 0V			180		μA
Quiescent Current		Switching, no load			26		mA
Power Output		f = 1kHz, THD+N = 10%, 4Ω Load			19.3		W
		f = 1kHz, THD+N = 10%, 8Ω Load			10.6		W
THD+ Noise		P_{OUT} = 1W, f = 1kHz, 4Ω Load			0.02		%
		P_{OUT} = 1W, f = 1kHz, 8Ω Load			0.02		%
Efficiency		f = 1kHz, P_{OUT} = 19.3W, 4Ω Load			91		%
		f = 1kHz, P_{OUT} = 10.6W, 8Ω Load			96		%
Maximum Power Bandwidth					20		kHz
Dynamic Range					97		dB
Noise Floor		A-Weighted			103		μV
Power Supply Rejection		V_{CC}=24V, Gain=8.25V/V, V_{RIPPLE}=200mV_{PP} C_R=100μF	f = 1kHz		-59		dB
			f = 217Hz		-59		dB

Circuit of figure 6, bridge-tied-load output configuration, V_{DD} = 24V, Gain=15V/V, V_{EN} = 5V, T_A = +25°C, unless otherwise noted.

Parameters	Symbol	Condition		Min	Typ	Max	Units
Standby Current		VEN = 0V			180		μA
Quiescent Current		Switching, no load			26		mA
Power Output		f = 1kHz, THD+N = 10%, 6Ω Load			50		W
		f = 1kHz, THD+N = 10%, 8Ω Load			40		W
THD+ Noise		P_{OUT} = 1W, f = 1kHz, 6Ω Load			0.04		%
		P_{OUT} = 1W, f = 1kHz, 8Ω Load			0.03		%
Efficiency		f = 1kHz, P_{OUT} = 50W, 6Ω Load			91		%
		f = 1kHz, P_{OUT} = 40W, 8Ω Load			94		%
Maximum Power Bandwidth					20		kHz
Dynamic Range					107		dB
Noise Floor		A-Weighted			140		μV
Power Supply Rejection		V_{CC}=24V, Gain=15V/V, V_{RIPPLE}=200mV_{PP}	f = 1kHz		-60		dB
			f = 217Hz		-60		dB

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PIN FUNCTIONS

Pin #	Name	Description
1, 14	N/C	Not connected internally
2	REF1	Internal analog reference (VDD/2) for Amplifier 1. For SE configuration, connect a bypass capacitor from REF1 to AGND (10μF).
3	IN1	Inverting input for amplifier 1.
4	TIMER1	Internal timer input for Amplifier 1. Connect a capacitor from TIMER1 to AGND (2.2μF) to set the internal timer for startup pop elimination.
5	AGND1	Analog ground for Amplifier 1. Connect AGND1 to AGND2. Connect PGND to AGND at a single point.
6	EN1	Enable input for Amplifier 1. Drive EN1 high to turn on the Amplifier 1, low to turn it off.
7	UVP1	Under-voltage protection reference input for Amplifier 1. Connect UVP1 to UVP2.
8	IN2	Inverting input for amplifier 2.
9	REF2	Internal analog reference (VDD/2) for Amplifier 2. For SE configuration, connect a bypass capacitor from REF2 to AGND (10μF).
10	TIMER2	Internal timer input for Amplifier 2. Connect a capacitor from TIMER2 to AGND (2.2uF) to set the internal timer for startup pop elimination.
11	AGND2	Analog ground for Amplifier 2. Connect AGND2 to AGND1. Connect PGND to AGND at a single point.
12	EN2	Enable input for Amplifier 2. Drive EN2 high to turn on the Amplifier 2, low to turn it off.
13	UVP2	Under-voltage protection reference input for Amplifier 2. Connect UVP2 to UVP1.
15, 16	VDD2	Power supply input for Amplifier 2. Bypass VDD2 to PGND2 with a 1μF X7R capacitor (in addition to the main bulk capacitor), placed close to the VDD2 and PGND2 pins.
17	BST2	High-side MOSFET bootstrap input for Amplifier 2. A capacitor from BST2 to SW2 supplies the gate drive current to the internal high-side MOSFET.
18, 19	SW2	Switched power output for Amplifier 2.
20, 21	PGND2	Power ground for Amplifier 2. Connect PGND2 to PGND1. Connect PGND to AGND at a single point.
22, 23	VDD1	Power supply input for Amplifier 1. Bypass VDD1 to PGND1 with a 1μF X7R capacitor (in addition to the main bulk capacitor), placed close to the VDD1 and PGND1 pins.
24	BST1	High-side MOSFET bootstrap input for Amplifier 1. A capacitor from BST1 to SW1 supplies the gate drive current to the internal high-side MOSFET.
25, 26	SW1	Switched power output for Amplifier 1.
27, 28	PGND1	Power ground for Amplifier 1. Connect PGND1 to PGND2. Connect PGND to AGND at a single point.
	Exposed Pad	Connect exposed pad to GND plane for proper thermal performance.

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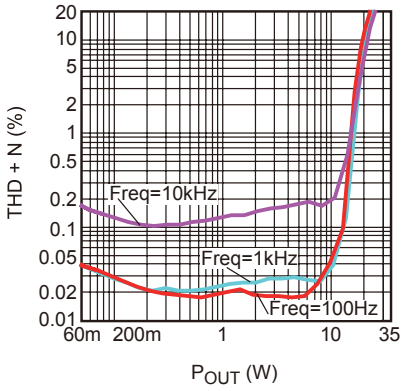
TYPICAL PERFORMANCE CURVES

Circuit of Figure 5, single-ended output configuration, V_{DD}=24V, V_{EN}=5V, A_V=8.25V/V, T_A = +25°C, unless otherwise noted.

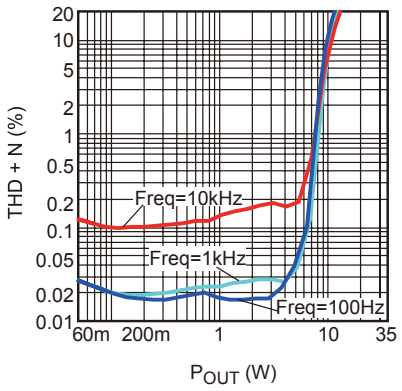
THD+N vs. Pout

V_{DD}=24V, R_{LOAD}=4Ω(SE)



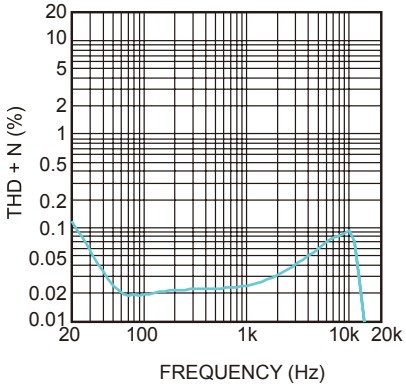
THD+N vs. Pout

V_{DD}=24V, R_{LOAD}=8Ω(SE)



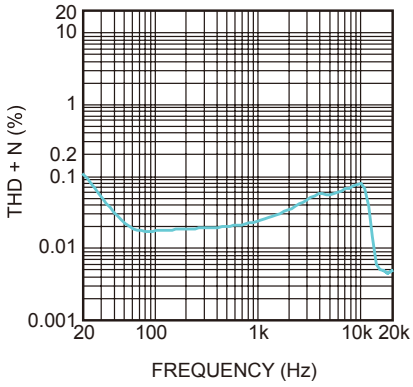
THD+N vs. Frequency

V_{DD}=24V, R_{LOAD}=4Ω(SE), P_{OUT}=1W



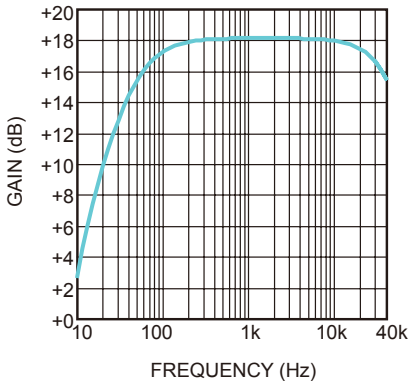
THD+N vs. Frequency

V_{DD}=24V, R_{LOAD}=8Ω(SE), P_{OUT}=1W



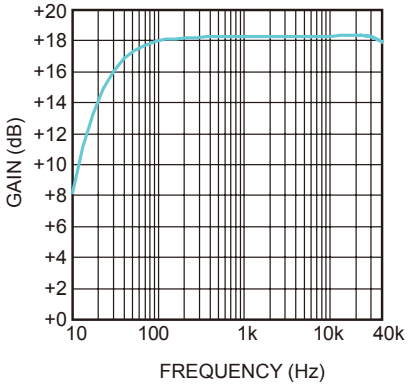
Frequency Response

V_{DD}=24V, R_{LOAD}=4Ω(SE), V_{IN}=250mV_{RMS}



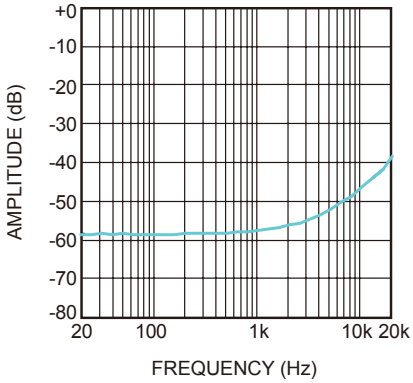
Frequency Response

V_{DD}=24V, R_{LOAD}=8Ω(SE), V_{IN}=250mV_{RMS}



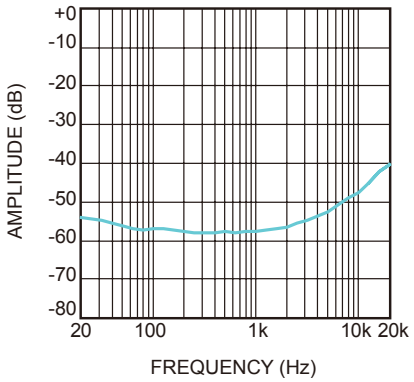
Power Supply Rejection Ratio

V_{DD}=24V, C_{BYP}=1µF, R_{LOAD}=4Ω(SE),
V_{RIPPLE}=0.3V_{PP}, C_R=100µF,
Input AC grounded



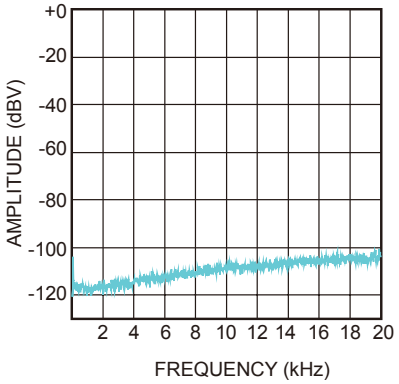
Power Supply Rejection Ratio

V_{DD}=24V, C_{BYP}=1µF, R_{LOAD}=8Ω(SE),
V_{RIPPLE}=0.3V_{PP}, C_R=100µF,
Input AC grounded



FFT Noise Floor

V_{DD}=24V, R_{LOAD}=4Ω(SE)



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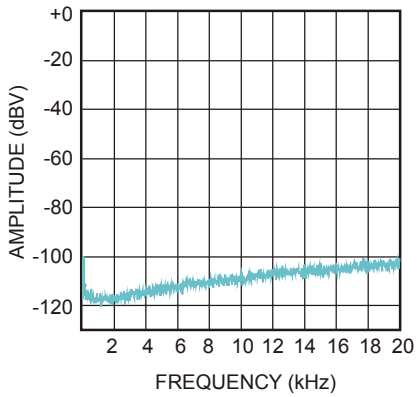
TYPICAL PERFORMANCE CURVES *(continued)*

Circuit of Figure 5, single-ended output configuration, V_{DD}=24V, V_{EN}=5V, A_V=8.25V/V, T_A = +25°C, unless otherwise noted.

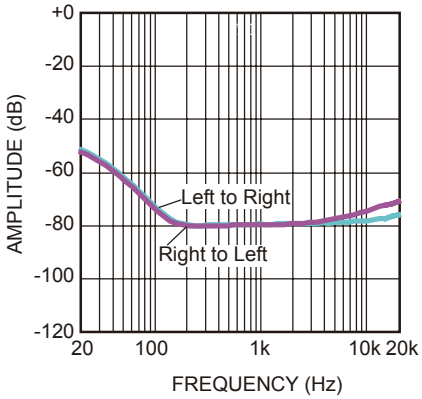
FFT Noise Floor

V_{DD}=24V, R_{LOAD}=8Ω(SE)



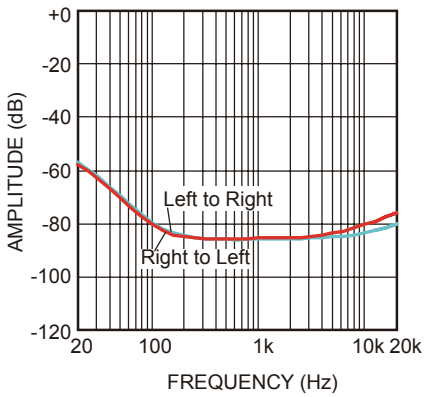
Cross Talk

V_{DD}=24V, R_{LOAD}=4Ω(SE), P_{OUT}=5W



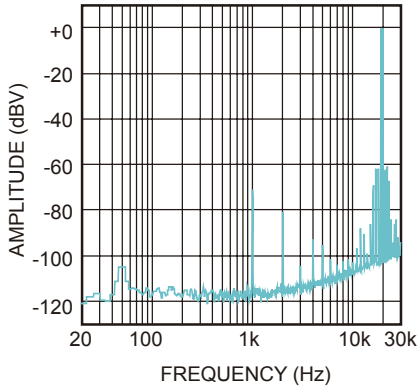
Cross Talk

V_{DD}=24V, R_{LOAD}=8Ω(SE), P_{OUT}=5W



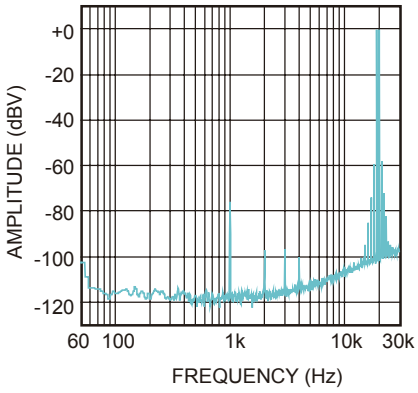
IHF-IMD

V_{DD} = 24V, R_{LOAD} =4Ω(SE),
Test Tones: 19kHz and 20kHz
Ratio=1:1



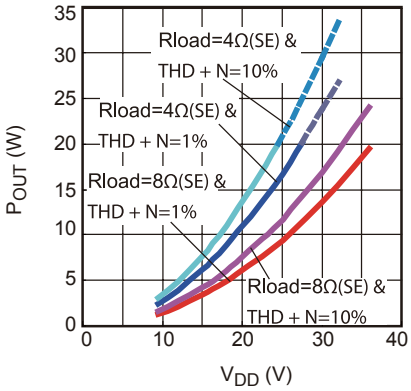
IHF-IMD

V_{DD} = 24V, R_{LOAD} =8Ω(SE),
Test Tones: 19kHz and 20kHz
Ratio=1:1



P_{OUT} vs. V_{DD}

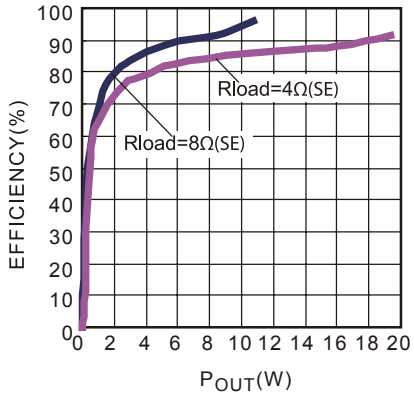
Input Signal Frequency =1kHz
the same P_{OUT} for both channels



Note: Dashed Lines represent thermally limited regions.

Efficiency vs. P_{OUT}

V_{DD} = 24V,
Input Signal Frequency=1kHz



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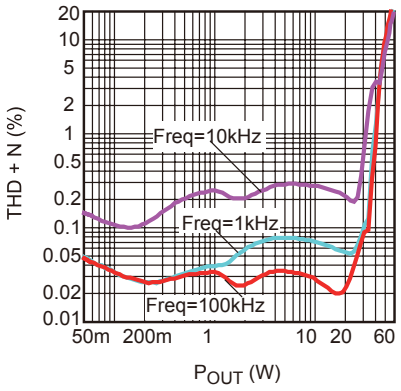
TYPICAL PERFORMANCE CURVES *(continued)*

Circuit of Figure 6, BTL output configuration, V_{DD}=24V, V_{EN}=5V, A_V=15V/V, T_A = +25°C, unless otherwise noted.

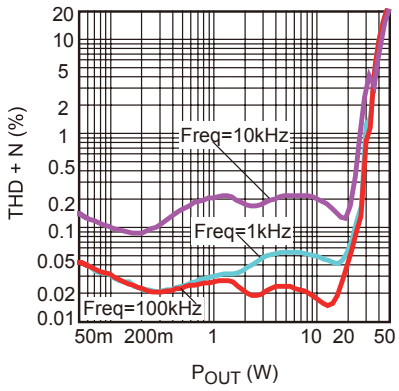
THD+N vs. Pout

V_{DD}=24V, R_{LOAD}=6Ω(BTL)



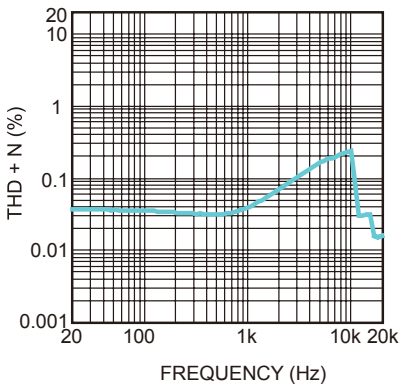
THD+N vs. Pout

V_{DD}=24V, R_{LOAD}=8Ω(BTL)



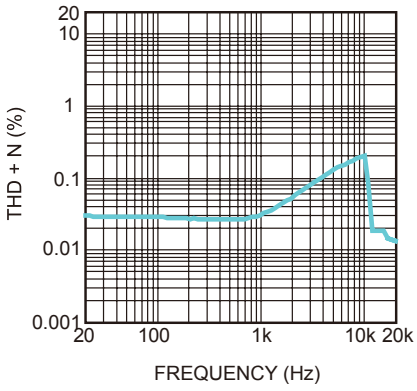
THD+N vs. Frequency

V_{DD}=24V, R_{LOAD}=6Ω(BTL), P_{OUT}=1W



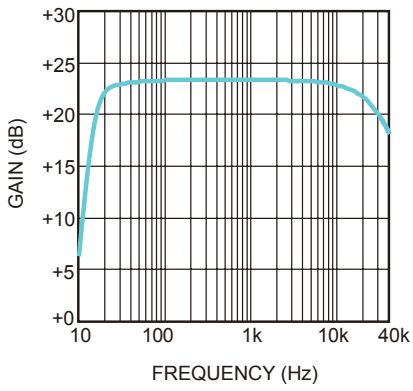
THD+N vs. Frequency

V_{DD}=24V, R_{LOAD}=8Ω(BTL), P_{OUT}=1W



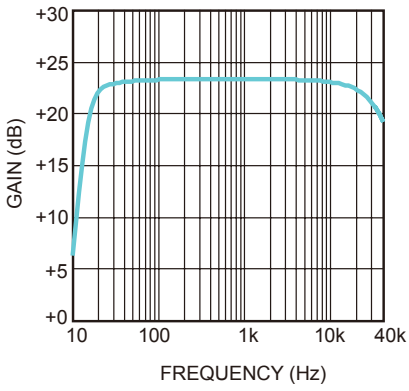
Frequency Response

V_{DD}=24V, R_{LOAD}=6Ω(BTL)



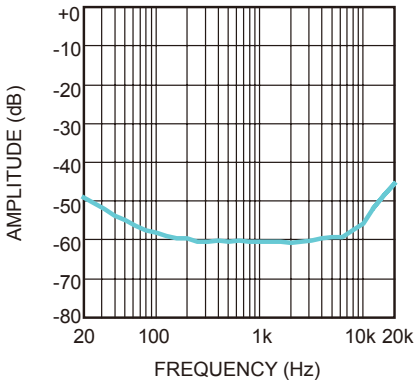
Frequency Response

V_{DD}=24V, R_{LOAD}=8Ω(BTL)



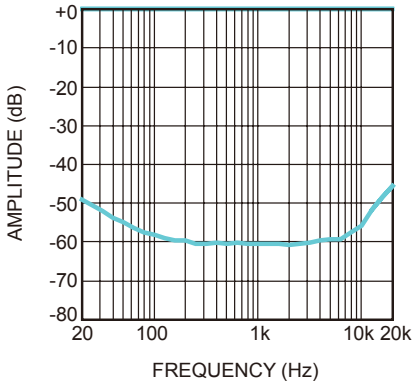
Power Supply Rejection Ratio

V_{DD}=24V, C_{BYP}=1µF, R_{LOAD}=6Ω(BTL),
V_{RIPPLE}=0.3V_{PP}, Input AC grounded



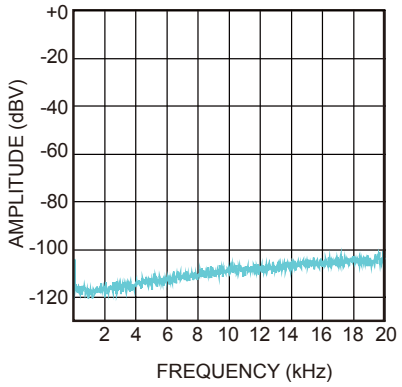
Power Supply Rejection Ratio

V_{DD}=24V, C_{BYP}=1µF, R_{LOAD}=8Ω(BTL),
V_{RIPPLE}=0.3V_{PP}, Input AC grounded



FFT Noise Floor

V_{DD}=24V, R_{LOAD}=6Ω(BTL)



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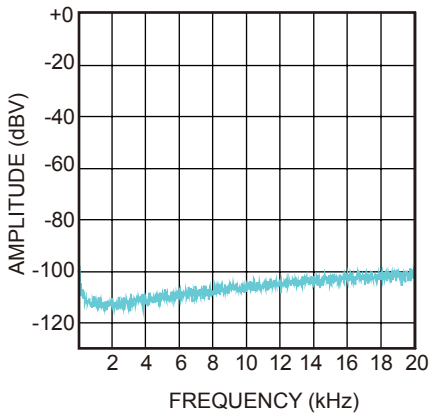
TYPICAL PERFORMANCE CURVES *(continued)*

Circuit of Figure 6, BTL output configuration, V_{DD}=24V, V_{EN}=5V, A_V=15V/V, T_A = +25°C, unless otherwise noted.

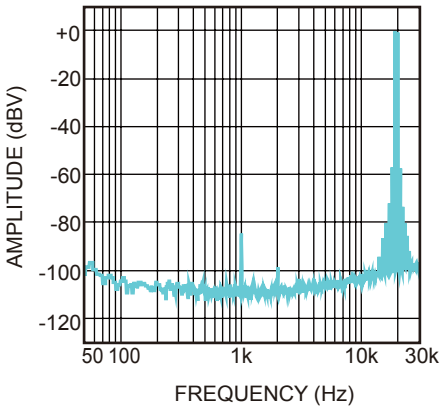
FFT Noise Floor

V_{DD}=24V, R_{LOAD}=8Ω(BTL)



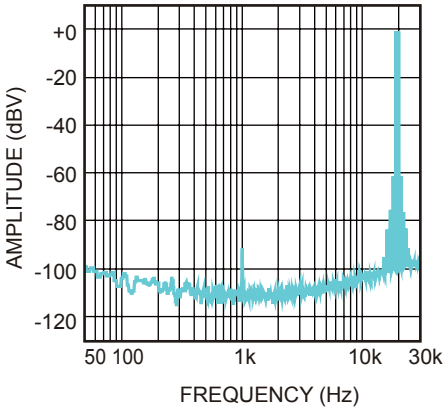
IHF-IMD

V_{DD} = 24V, R_{LOAD} =6Ω(BTL),
Test Tones: 19kHz and 20kHz
Ratio=1:1



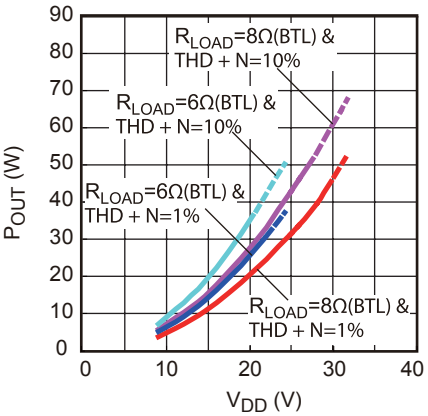
IHF-IMD

V_{DD} = 24V, R_{LOAD} =8Ω(BTL),
Test Tones: 19kHz and 20kHz
Ratio=1:1



P_{OUT} vs. V_{DD}

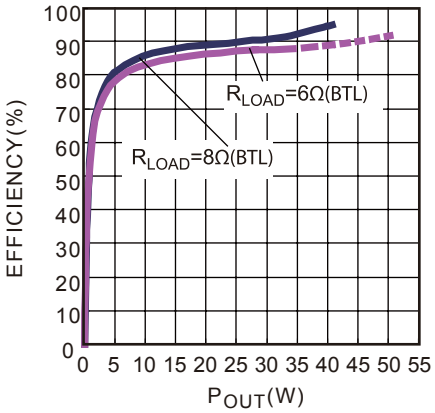
Input Signal Frequency =1kHz



Note: Dashed Lines represent thermally limited regions.

Efficiency vs. P_{OUT}

V_{DD} = 24V,
Input Signal Frequency=1kHz



Note: Dashed Line represents with external heat-sink

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BLOCK DIAGRAM

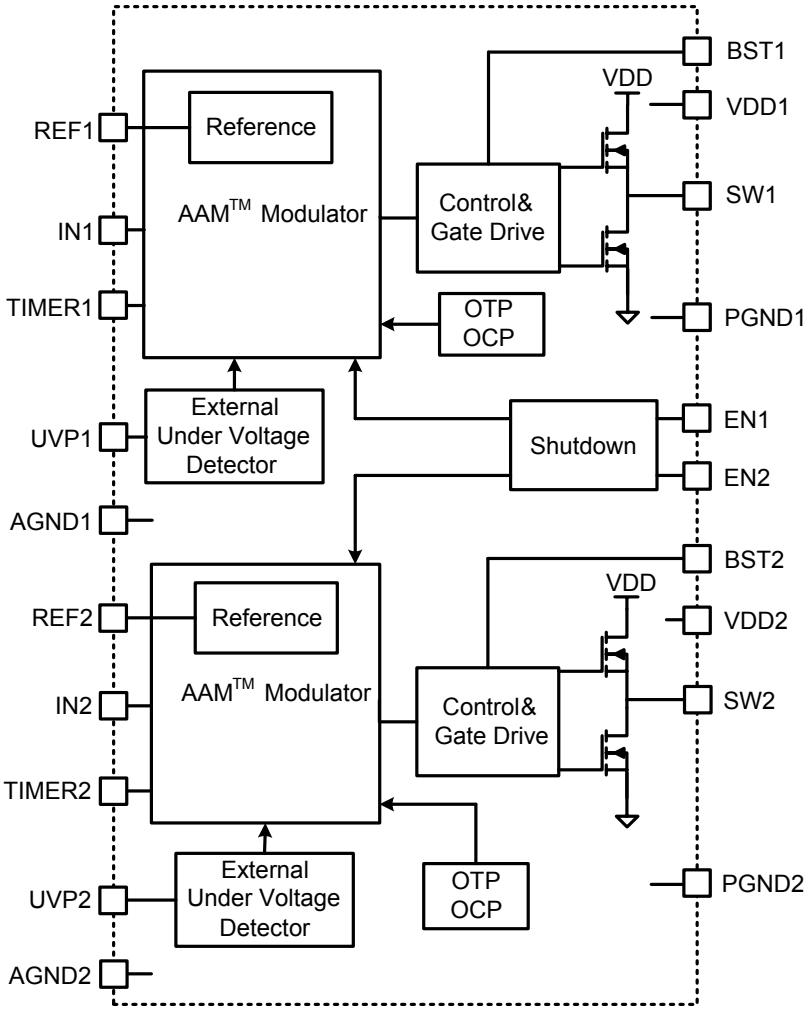

Figure1—Function block Diagram

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OPERATION

The MP7748 is a Class D Audio Amplifier for driving stereo speakers in single-ended configuration or a mono speaker in bridge-tied-load configuration. It uses the Monolithic Power Systems patented Analog Adaptive Modulation™ to convert the audio input signal into pulses. These pulses drive an internal high-current output stage and, when filtered through an external inductor-capacitor filter, reproduce the input signal across the load. Because of the switching Class D output stage, power dissipation in the amplifier is drastically reduced when compared to Class A, B or A/B amplifiers while maintaining high fidelity and low distortion.

REF1/2 are the positive inputs of the two amplifiers. They are set to half the DC power supply input voltage (V_{DD}/2) by the internal circuit. The input capacitor C_{IN} couple the AC signal at the input.

The amplifier voltage gain is set by the combination of the input resister $R_{IN1/2}$ and the feedback resistor $R_{FB1/2}$ and is calculated by the equation:

$$AV = \frac{-R_{FB}}{R_{IN}}$$

The MP7748 includes four high-power MOSFETs wherein for each channel the output driver stage uses two 250mΩ N-channel MOSFETs to deliver the pulses to the LC output filter which in turn drives the load. To fully enhance the high-side MOSFET, the gate is driven to a voltage higher than the source by the bootstrap capacitor between SW and BS. While the output is driven low, the bootstrap capacitor is charged from V_{DD} through an internal circuit on the MP7748. The gate of the high-side MOSFET is driven high from the voltage at BS, forcing the MOSFET gate to a voltage higher than V_{DD} and allowing the MOSFET to fully turn on, reducing power loss in the amplifier.

Pop Elimination

The MP7748 integrates a source current function to charge the AC coupling capacitor $C_{OUT1/2}$ for the SE output configuration and $C_{IN1/2}$ at the start up moment. The start up source current slew rate is adjustable by selecting different capacitance of timer capacitor $C_{TIMER1/2}$. The larger the capacitance of the timer capacitor is, the smaller the start up current slew rate is. The recommended 2.2μF timer capacitor results in a start up current slew rate of approximately 20mA/350ms which would help to minimize the turn on pop.

After driving EN pin low, output SW will be set to high impedance immediately which would help to eliminate the turn off pop.

Short Circuit/Overload Protection

The MP7748 has internal overload and short circuit protection. The currents in both the high-side and low-side MOSFETs are measured and if the current exceeds the 4.5A short circuit current limit, both MOSFETs are turned off. The MP7748 then restarts with the same power up sequence that is used for normal starting to prevent a pop from occurring after a short circuit condition is removed.

Enable Function

The MP7748 EN input is an active high enable control. To enable the MP7748, drive EN with a 2.0V or higher voltage. To disable the amplifier, drive it below 0.4V. While the MP7748 is disabled, the VDD operating current is less than 140μA and the output driver MOSFETs are turned off.

Programmable UVP

MP7748 integrate programmable UVP function, which can be used to shutdown the MP7748 to escape the pop, by controlling the UVP node voltage. The corresponding circuit is shown in the followed figure 2. If the UVP pin is NC, the default VDD shutdown voltage (rising threshold) is 8.4V since there is internal voltage divided circuit. The VDD shutdown voltage can be flexibly adjusted by controlling UVP pin voltage The recommended VDD shutdown voltage is from 9.5V to power supply. As shown in the figure 2, if external resistor R_H and R_L is low enough (e.g. R_H, R_L < 50kΩ) compared with internal 500kΩ and 550kΩ resistor, the VDD shutdown voltage (rising threshold) can be calculated by the equation:

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$$V_{VDD_shutdown} = 4 * \frac{(R_H + R_L)}{R_L}$$

The hysteresis voltage can be calculated by the equation：

$$V_{hysteresis} = 10\% * V_{VDD_shutdown}$$

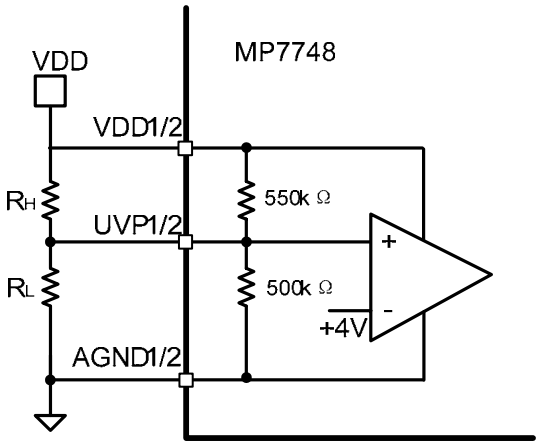

Figure 2—UVP block diagram

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APPLICATION INFORMATION

Component Selection

The MP7748 uses a minimum number of external components to complete a stereo SE or mono BTL Class D audio amplifier. The circuit of Figure 3 (stereo SE application circuit) and figure 4 (mono BLT application circuit) are optimized for a 24V power supply. This circuit should be suitable for most applications, and use the following sections to determine how to customize the amplifier for a particular application.

Setting the Voltage Gain

The maximum output voltage swing is limited by the power supply. To achieve the maximum power out of the MP7748 amplifier, set the gain such that the maximum input signal results in the maximum output voltage swing.

For single-ended (SE) output configuration, the maximum output voltage $V_{OUT(PK)}$ is $V_{DD}/2$. For bridge-tied-load (BTL) output configuration, the maximum output voltage $V_{OUT(PK)}$ is V_{DD}. For a given input signal voltage, where $V_{IN(PK)}$ is the peak input voltage, the maximum voltage gain is:

$$A_V(MAX) = \frac{V_{OUT(PK)}}{V_{IN(PK)}}$$

This voltage gain setting results in the peak output voltage approaching it's maximum for the maximum input signal. In some cases the amplifier is allowed to overdrive slightly, allowing the THD to increase at high power levels, and so a higher gain than A_V (max) is required.

Setting the Switching Frequency

The idle switching frequency (the switching frequency when no audio input is present) is a function of several variables: the supply voltage V_{DD}, the integral capacitor C_{INT} and the feedback resistor R_{FB}. Lower switching frequency results in more inductor ripple, causing more quiescent output voltage ripple and increasing the output noise and distortion. Higher switching frequencies result in more power loss. The optimum quiescent switching frequency is approximately 600kHz. When used to drive stereo speakers in single-ended configuration, it is recommended to set right channel idle switching frequency larger than left channel's with 50k Hz difference by using different timing capacitor C_{INT}. For detailed please refer to the table 1 for recommended SE output configuration design, and table 2 for recommended BTL output configuration design.

Table 1—Switching Frequency Setting For SE Output Configuration

V_{DD} (V)	Gain (V/V)	R_{FB} (kΩ)	R_{IN} (kΩ)	Left channel		Right channel	
				C_{INT1} (nF)	F_{SW1} (kHz)	C_{INT2} (nF)	F_{SW2} (kHz)
12	5.6	56	10	4.7	560	3.3	700
12	8.2	39	4.7	5.6	620	4.7	700
12	12.0	56.4	4.7	4.7	530	3.3	670
12	17.6	56.4	3.2	4.7	530	3.3	670
12	25.5	56.4	2.2	4.7	530	3.3	670
12	30	60	2	4.7	520	3.3	650
24	5.6	56	10	10	540	8.2	650
24	8.2	82	10	5.6	610	4.7	690
24	12.0	120	10	4.7	530	3.3	660
24	17.4	82	4.7	5.6	610	4.7	690
24	25.5	120	4.7	4.7	530	3.3	660
24	30	120	4	4.7	530	3.3	660

Table 2 - Switching Frequency Setting For BTL Output Configuration

V_{DD} (V)	Gain (V/V)	R_{FB} (kΩ)	R_{IN} (kΩ)	C_{INT1} (nF)	F_{SW1} (kHz)
12	10	100	10	3.9	400
12	20	100	5	3.3	400
12	30	121	4.02	2.7	400
24	10	100	10	3.9	580
24	20	121	6.04	3.9	480
24	30	121	4.02	3.9	480
32	10	100	10	4.7	580
32	20	121	6.04	3.9	560
32	30	162	5.36	3.3	500

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Choosing the Output LC Filter

The Inductor-Capacitor (LC) filter converts the pulse train at SW to the output voltage that drives the speaker. There are two kinds of LC filter structure depending on the output configuration.

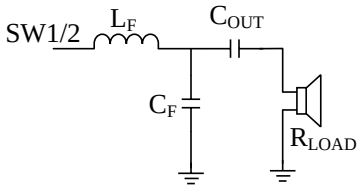

Figure 3—SE Filter Configuration

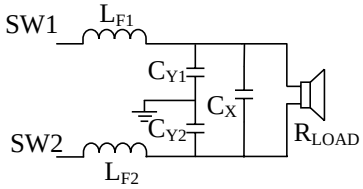

Figure 4—BTL Filter Configuration

Where:

$$L_F = L_{F1} + L_{F2},$$

$$C_F = C_X + \frac{C_{Y1} \times C_{Y2}}{C_{Y1} + C_{Y2}},$$

$$L_{F1} = L_{F2};$$

$$C_{Y1} = C_{Y2}$$

The characteristic frequency of the LC filter needs to be high enough to allow high frequency audio to the output, yet needs to be low enough to filter out high frequency products of the pulses from SW. The characteristic frequency of the LC filter is:

$$f_0 = \frac{1}{2 \times \pi \times \sqrt{L_F \times C_F}}$$

The quality factor (Q) of the LC filter is important. If this is too low, output noise will increase, if this is too high, then peaking may occur at high signal frequencies reducing the passband flatness. The circuit Q is set by the load resistance (speaker resistance, typically 4Ω or 8Ω). The Q is calculated as:

$$Q = \frac{R_{LOAD}}{\omega_0 \times L_F} = \frac{R_{LOAD}}{2\pi \times f_0 \times L_F}$$

ω_0 is the characteristic frequency in radians per second and f_0 is in Hz. Use an LC filter with Q between 0.7 and 1.

The actual output ripple and noise is greatly affected by the type of inductor and capacitor used in the LC filter. Use a film capacitor and an inductor with sufficient power handling capability to supply the output current to the load. The inductor should exhibit soft saturation characteristics. If the inductor exhibits hard saturation, it should operate well below the saturation current. Gapped ferrite, MPP, Powdered Iron, or similar type toroidal cores are recommended. If open or shielded bobbin ferrite cores are used for multi-channel designs, make sure that the start windings of each inductor line up (all starts going toward SW pin, or all starts going toward the output) to prevent crosstalk or other channel-to-channel interference.

Output Coupling Capacitor For SE Output

The output AC coupling capacitor C_{OUT} serves to block DC voltages and thus passes only the amplified AC signal from the LC filter to the load. The combination of the coupling capacitor, C_{OUT} and the load resistance results in a first-order high-pass filter. The value of C_{OUT} should be selected such that the required minimum frequency is still allowed to pass. The output corner frequency (-3dB point), f_{OUT}, can be calculated as:

$$f_{OUT} = \frac{1}{2 \times \pi \times R_{LOAD} \times C_{OUT}}$$

Set the output corner frequency (f_{OUT}) at or below the minimum required frequency.

The output coupling capacitor carries the full load current, so a capacitor should be chosen such that its ripple current rating is greater than the maximum load current. Low ESR aluminum electrolytic capacitors are recommended.

Input Coupling Capacitor

The input coupling capacitors C_{IN1} and C_{IN2} are used to pass only the AC signal at the input. In a typical system application, the source input signal is typically centered around the circuit ground, while the MP7748 input is at half the power supply voltage (V_{DD}/2). The input coupling capacitor transmits the AC signal from the source

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to the MP7748 while blocking the DC voltage. Choose an input coupling capacitor such that the corner frequency (f_{IN}) is less than the passband frequency. The corner frequency is calculated as:

$$f_{IN} = \frac{1}{2 \times \pi \times R_{IN} \times C_{IN}}$$

Timer capacitor

The start up source current slew rate is adjustable by selecting different capacitance of timer capacitor C_{TIMER}. The larger the C_{TIMER} capacitance is, the smaller the start up current slew rate is. It is recommended to use the C_{TIMER} which capacitance is larger than 312nF, so the start up current slew rate would be smaller than 20mA/50ms which would help to eliminate the turn on pop. The recommended 2.2μF capacitor C_{TIMER} results in a start up current slew rate of approximately 20mA/350ms.

Power Source

For maximum output power, the amplifier circuit requires a regulated external power source to supply the power to the amplifier. The higher the power supply voltage, the more power can be delivered to a given load resistance, however if the power source voltage exceeds the maximum voltage of 36V, the MP7748 may sustain damage. The power supply rejection of the MP7748 is excellent, however noise at the power supply can get to the output, so care must be taken to minimize power supply noise within the pass-band frequencies. Bypass the power supply with a large capacitor (typically aluminum electrolytic) along with a smaller 1μF ceramic capacitor at the MP7748 V_{DD} supply pins.

PCB Layout

The circuit layout is critical for optimum performance and low output distortion and noise. It is highly recommended to duplicate EVB layout for optimum performance. If change is necessary, please follow these guidelines and take Figure 7 for references.

1) Place the following components as close to the MP7748 as possible:

Bootstrap Cap

C_{BS1} and C_{BS2} are used to supply the gate drive current to the internal high-side MOSFET. Place C_{BS1} as close to BST1/2 pin and SW1/2 pin as possible. Likewise, place C_{BS2} as close to BST2 pin and SW2 pins as possible.

Power Supply Bypass Cap

C_{BYP1} and C_{BYP2} carry the transient current for the switching power stage. To prevent overstressing of the MP7748 and excessive noise at the output, place C_{BYP1} as close to VDD1 pins and PGND1 pins as possible and also place C_{BYP2} as close to VDD2 pins and PGND2 pins as possible.

Integral Capacitors

C_{INT} are used to set the amplifier switching frequencies and are typically on the order of a few nF. Place the integral capacitor C_{INT} as close to the corresponding input as possible to reduce distortion and noise. For example, place C_{INT1} as close to pins 2 and 3 as possible at SE output configuration.

Reference Bypass Capacitors For SE Output

When used with SE output, CR1 and CR2 is needed to filter the ½ VDD reference voltages. Place C_{R1} and C_{R2} as close to the IC as possible to improve power supply rejection and reduce distortion and noise at the output.

2) The Inductor-Capacitor (LC) filter converts the pulse train at SW to the output voltage that drives the speaker. Please keep the filter capacitor close to the inductor.

3) When laying out the PCB, use two separate ground planes, analog ground (AGND) and power ground (PGND), and connect the two grounds together at a single point (usually around the bulk bypass capacitor) to prevent noise injection into the amplifier input to reduce distortion.

4) Keep the sensitive feedback signal trace on the input side and shield the trace with the AGND plane. Make sure that any traces carrying the switch node (SW) voltages are separated far from any input signal traces. If it is required to run the SW trace near the input, shield the input with a ground plane between the traces. Make sure that each channel is physically separated to prevent crosstalk. Make sure that all inductors used on a single circuit board have the same orientation.

Also, make sure that the power supply is routed from the source to each channel individually, not serially. This prevents channel-to-channel

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coupling through the power supply input.

Electro-Magnetic Interference (EMI) Considerations

Due to the switching nature of the Class D amplifier, care must be taken to minimize the effects of electromagnetic interference from the amplifier. However, with proper component selection and careful attention to circuit layout, the effects of the EMI due to the amplifier switching can be minimized.

The power inductors are a potential source of radiated emissions. For the best EMI performance, use toroidal inductors, since the magnetic field is well contained inside the core. However toroidal inductors can be expensive to wind. For a more economical solution, use shielded gapped ferrite or shielded ferrite bobbin core inductors. These inductors typically do not contain the field as well toroidal inductors, but usually can achieve a better balance of good EMI performance with low cost.

The size of high-current loops that carry rapidly changing currents needs to be minimized. To do this, make sure that the V_{DD} bypass capacitors are as close to the MP7748 as possible.

Nodes that carry rapidly changing voltage, such as SW, need to be made as small as possible. If sensitive traces run near a trace connected to SW, place a ground shield between the traces.

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YPICAL APPLICATION CIRCUIT

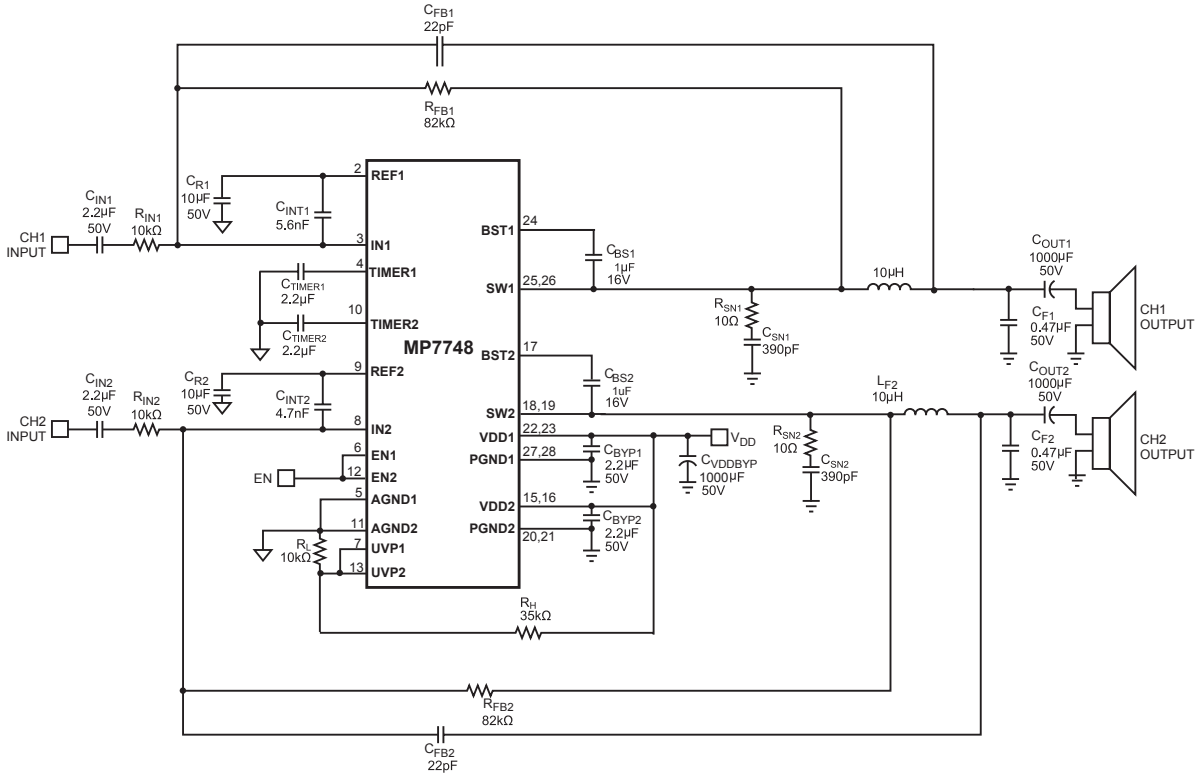

Figure 5—24V VDD Stereo SE Typical Application Circuit

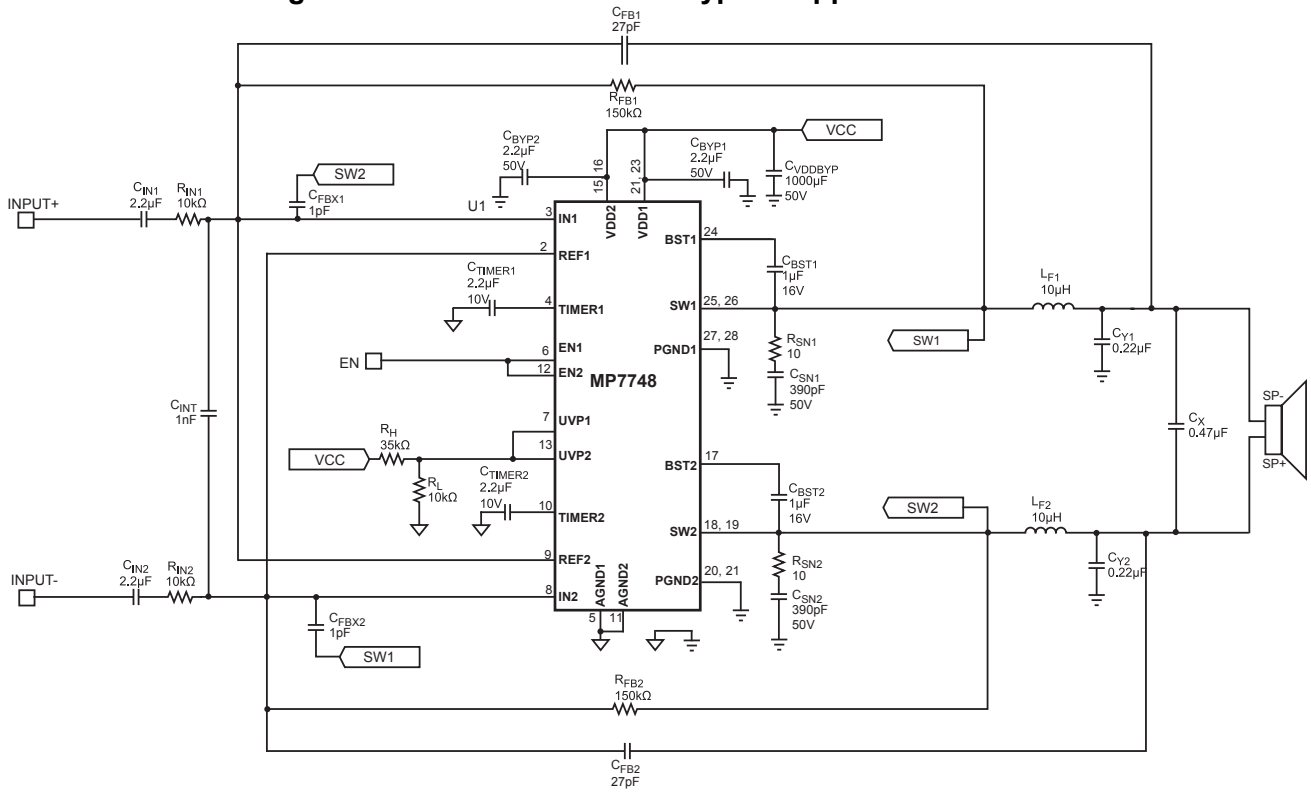

Figure 6—24V VDD mono BTL Typical Application Circuit

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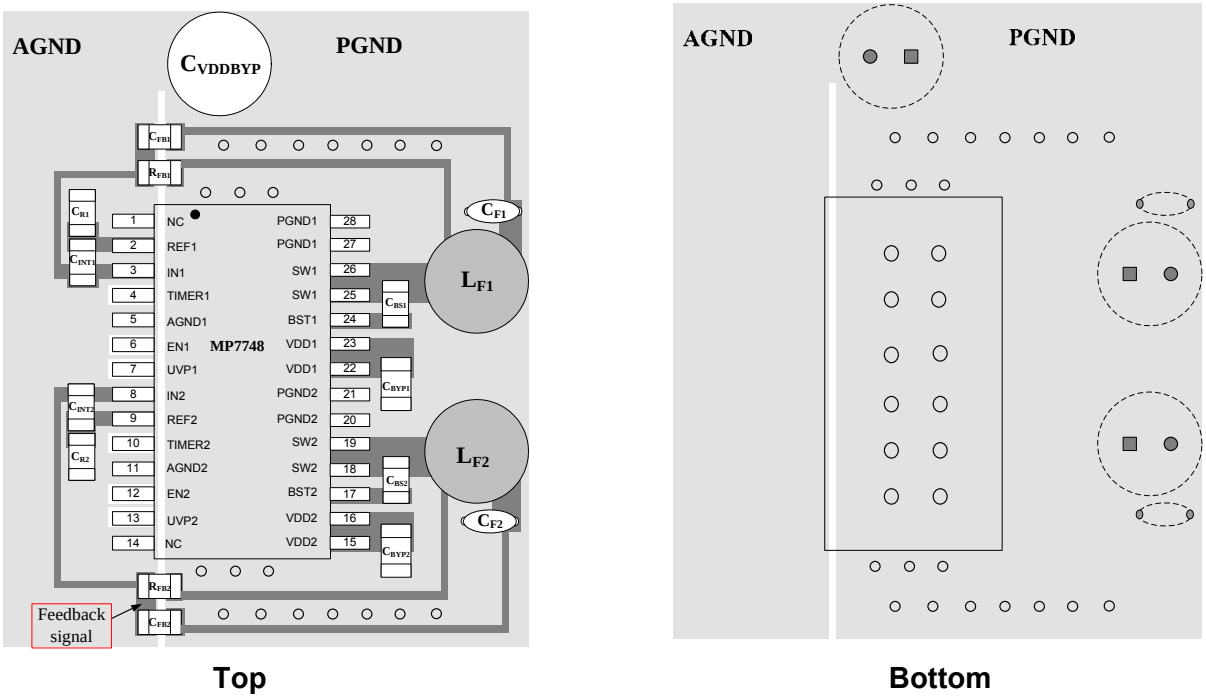

Figure 7—Stereo SE Reference PCB Layout

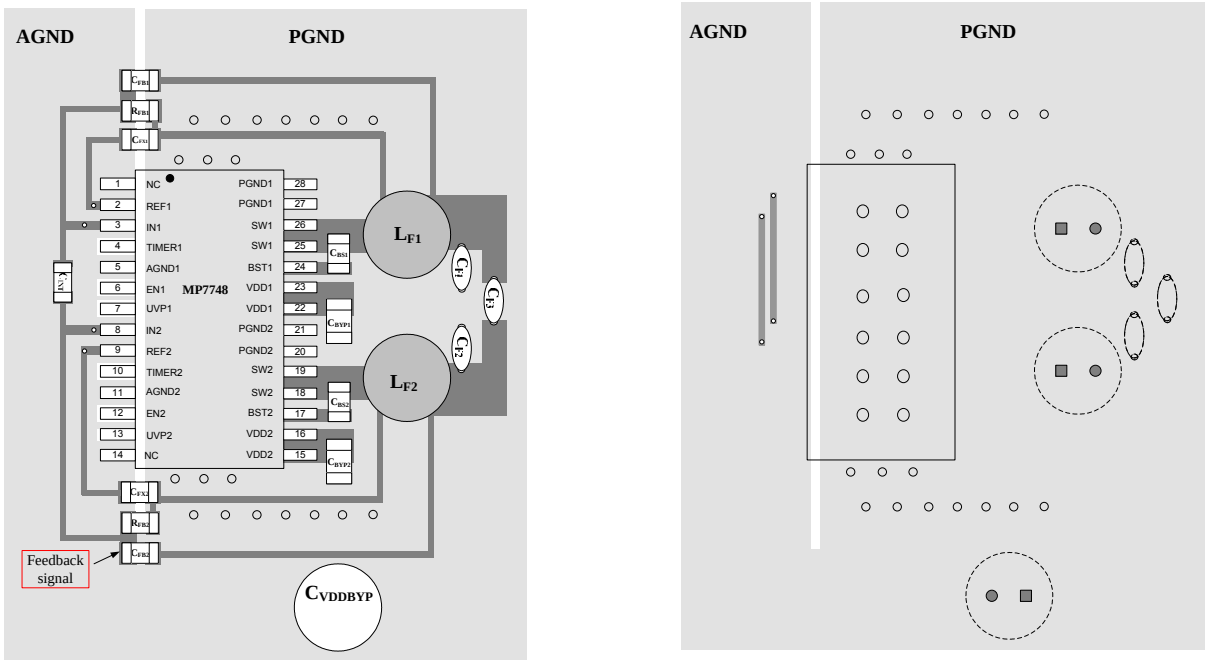

Figure 8—Mono BTL Reference PCB Layout

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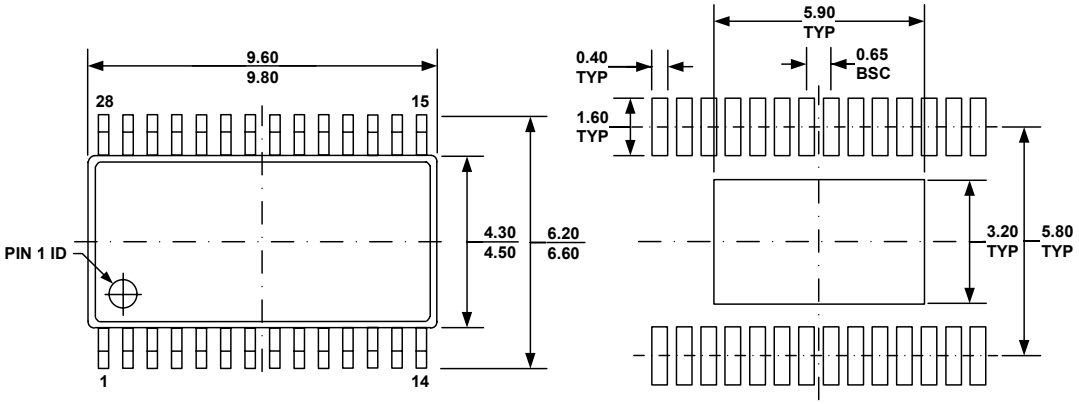
PACKAGE INFORMATION

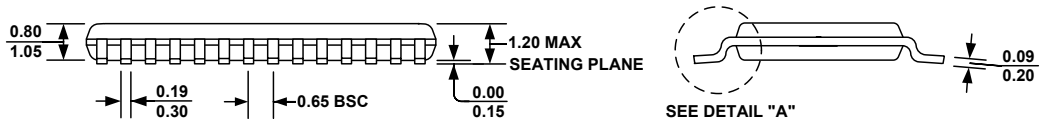
TSSOP28

PACKAGE OUTLINE DRAWING FOR 28-TSSOP w/ EXPOSED PADDLE



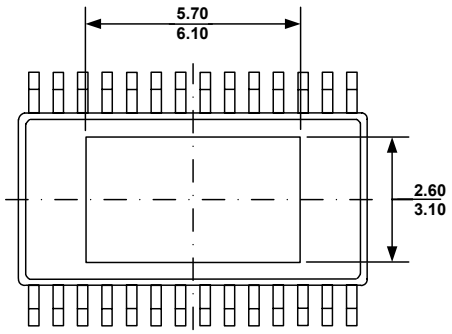
TOP VIEW

RECOMMENDED LAND PATTERN

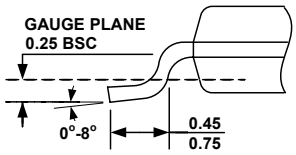


FRONT VIEW

SIDE VIEW



BOTTOM VIEW



DETAIL “A”

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В нашем ассортименте представлены ведущие мировые производители активных и пассивных электронных компонентов.

Нашей специализацией является поставка электронной компонентной базы двойного назначения, продукции таких производителей как XILINX, Intel (ex.ALTERA), Vicor, Microchip, Texas Instruments, Analog Devices, Mini-Circuits, Amphenol, Glenair.

Сотрудничество с глобальными дистрибьюторами электронных компонентов, предоставляет возможность заказывать и получать с международных складов практически любой перечень компонентов в оптимальные для Вас сроки.

На всех этапах разработки и производства наши партнеры могут получить квалифицированную поддержку опытных инженеров.

Система менеджмента качества компании отвечает требованиям в соответствии с ГОСТ Р ИСО 9001, ГОСТ РВ 0015-002 и ЭС РД 009

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