

LED Drivers for Automotive Light

BD8381AEFV-M

General Description

BD8381AEFV-M is a white LED driver with the capability of withstanding high input voltage (50V MAX). It has also an integrated current-mode, buck-boost DC/DC controller to achieve stable operation against high input voltage and to remove the constraint of the number of LEDs in series connection.

The LED brightness is controlled by either linear or PWM signal and is also possible to be controlled even without using a microcomputer, but instead, by means of the built-in PWM brightness signal generation circuit.

Features

- Integrated buck-boost current-mode DC/DC controller
- Built-in CR timer for PWM brightness
- **PWM** linear brightness
- Built-in protection functions (UVLO, OVP, TSD, OCP, SCP)
- LED error status detection function (OPEN/ SHORT)

Applications

Headlight and Daytime Running Light etc.

Typical Application Circuit and Block Diagram

Key Specifications

- Input Supply Voltage Range: 5.0V to 30V
■ Operating Temperature Range: 40°C to +125°C
- Operating Temperature Range:

Package W(Typ) x D(Typ) x H(Max)

〇Product structure: Silicon monolithic integrated circuit 〇This product has no designed protection against radioactive rays

Pin Configuration

Pin Descriptions

Absolute Maximum Ratings (Ta=25°C)

(Note 1) IC mounted on glass epoxy board measuring 70mm x 70mm x 1.6mm, power dissipated at a rate of 11.60mW/°C at temperatures above 25°C. Caution: Operating the IC over the absolute maximum ratings may damage the IC. The damage can either be a short circuit between pins or an open circuit
between pins and the internal circuitry. Therefore, it is important to over the absolute maximum ratings..

Recommended Operating Conditions (Ta=25°C)

(Note 2) Connect SYNC to GND or OPEN when not using external frequency synchronization.

(Note 3) Do not switch between internal and external synchronization when an external synchronization signal is input to the device.

Electrical Characteristics (Unless otherwise specified, V_{CC}=12V Ta=25°C)

Typical Performance Curves

(Unless otherwise specified, Ta=25°C)

Figure 2. Oscillating Frequency vs Temperature $(f_{OSC}$ Temperature Characteristic)

Figure 4. Circuit Current vs Power Supply Voltage

(Unless otherwise specified, Ta=25°C)

Figure 6. Efficiency vs Power Supply Voltage (Input Voltage Dependence)

Figure 8. PWMOUT Output Voltage vs VTH Threshold Voltage

Datasheet

(Unless otherwise specified, Ta=25°C)

Figure 9. Output Voltage vs DRLIN Threshold Voltage Figure 10. Output Voltage vs EN Threshold Voltage

(DRLIN=VREG)

Figure 11. Output Voltage vs Temperature (VREG Voltage Temperature Characteristic)

Figure 12. Over-Voltage Detection Reference Voltage vs Temperature (OVP Voltage Temperature Characteristic)

Typical Performance Curves – continued

(Unless otherwise specified, Ta=25°C)

Figure 14. LED Short Detection Voltage vs **Temperature**

Application Information

1. Application Circuit

Application Circuit 1

Figure 15

Buck application composition (It is INP1, INP2 and two input selector function and EN connected direct to VCC)

Application Circuit 2

Figure 16 Boost application composition (When invalidating short detection and EN is inputted by a voltage divider)

2. Reference PCB Setting

Figure 17

(Note)

 When no PWM dimming, DI2 should be a schottky diode instead of a Fast Recovery diode to improve efficiency. When dimming with External PWM signal, DISC should be pulled up to VREG with 10KΩ, then input PWM signal to VTH.(when no PWM dimming, remove Q3 and replace $R_{Q3} = 0Ω$ and short to DS)

 Efficiency improvement is possible by making DI2 a schottky Diode .However, since high temperature leakage current is large and output voltage ripple is large as well, LED may flicker when PWM dimming ratio is very low. So it is recommended to use a Fast recovery Diode.

 Values of the capacitors can be smaller than the amount that was selected by the DC bias characteristics of the capacitor when using ceramic capacitors.

For EMI reduction, please insert resistance to ROUTL and RBOOT. It is recommended to be below 20Ω.

 The output voltage ripple is larger in Boost application than in Buck application. Hence, it is recommended to use at least 100µ F output capacitor.

3. 5V Voltage Reference (VREG)

5V (Typ) is generated from the VCC input voltage when the enable pin is set high. This voltage is used to power internal circuitry, as well as the voltage source for device pins that need to be fixed to a logical HIGH.

UVLO protection is integrated into the VREG pin. The voltage regulation circuitry operates uninterrupted for output voltages higher than 4.5 \check{V} (Typ), but if output voltage drops to 4.3 V (Typ) or lower, UVLO engages and turns the IC off. Connect a capacitor ($C_{REG} = 10 \mu$ F Typ) to the VREG terminal for phase compensation. Operation may become unstable if CREG is not connected.

Figure 18. LED current setting block diagram Figure 19. The LED current derating by THM terminal

(2) Linear dimming function

LED current can be controlled linearly by using the THM terminal which is commonly used as a derating function. For example, THM terminal is used when suppressing the degradation at high temperature of the LED (Figure 20) and controlling the excessive current to the external components under the conditions likely to occur in the power supply voltage fluctuations in the idling stop function. V_{THM} input range is recommended V_{THM} ≥ 0.4V.

Figure 20. The derating use case with thermistor resister.

5. Setting of CR Timer Dimming

It is possible to set the PWM frequency (f_{PWM}) and the PWM on Duty (DON) with the external resistor and capacitor by using the built-in CR timer function. This function can be used to set the Dimming range from 2%up to 45% and the frequency range from 100Hz up to 20kHz. When a Hi voltage is applied at DRLIN terminal, 100% On-Duty is outputted at the PWMOUT terminal and at the LED current, independent of the PWM signal and the CR Timer. The minimum PWM pulse width is 25μs.

Figure 21. The setting of PWM dimming using CR Timer and Timing chart

Synchronization of the PWM dimming signal with an external signal is possible by inputting the external signal at the VTH terminal. The Hi voltage of the external signal can be more than 3.7V and the Low voltage can be less than 1.0V.

6. Relationship between PWM dimming and SCP protection

If the PWM ON-Time is short, even if it is an internal or an external PWM dimming, it will cause the rise time of the output voltage to be delayed and there is likely to have a false detection of the SCP. Figure 23 and Figure 24 indicates the relation between SCP and PWM dumming. Detail explanation of SCP is described in P.16.

The rise time of the output voltage at PWM dimming is calculated as follows. The COMP voltage starts to increase when PWM=Hi and the switching output of the DC/DC circuit depends on the C_{PC} capacitor connected at the COMP terminal .It also affects the soft start time during start-up to prevent the rush current. (Refer to P.15 for more details.)

Base on the above explanation, the time (t_{UP}) it takes for the output voltage to reach the steady state level is calculated as follows.

$$
t_{UP} = t_{SS} + t_{COMP}
$$

$$
t_{SS} = \frac{V_{SWST}[V] \times C_{SS}[\mu F]}{I_{SS}[\mu A]}
$$

 $I_{COMPSOLRCE}[\mu A]$ *DON* $t_{COMP} = \frac{V_{SWMAX}[V] \times C_{PC}[\mu F]}{V_{VXX}}$ *COMPSOURCE* $\frac{V_{SWMAX}[V] \times C_{PC}[\mu] }{I} \times \frac{1}{P}$ $[\mu A]$ $=\frac{V_{SWMAX}[V]{\times}C_{PC}[\mu F]}{I_{COMPSOLRCE}[\mu A]} \times$ μ

Rise Time of COMP voltage : t_{COMP} COMP source current: I_{COMPSOURCE} Capacitor of COMP: C_{PC} Soft start time: tss SS Charged current: Iss Capacitor of SS: Css PWM Dimming rate: DON Soft start release voltage 0.85V (Max): t_{SWST} MaxDuty output voltage $2.0V$ (Max): V_{SWMAX}

During the rise time of the output voltage which is calculated above, SCP detection starts the timer operation which is synchronized with EN. If the PWM dimming ratio is low and the rise time of output voltage is delayed, there is a possibility for a false detection of SCP.

Ex)

The condition that $I_{COMPSOURCE}$ =75 μ A,C_{PC}=0.1 μ F, I_{SS} =5 μ A,C_{SS}=0.1 μ F, DON=5% are $t_{SS}=17$ ms, $t_{COMP}=53.3$ ms. So, t_{UP} is about 60ms

From the above, when using the PWM dimming, it must establish the below relationship. (tscp indicates the SCP mask time. It indicates P.16 in detail.)

t_{UP} < t_{SCP}

As a reference, it is recommended that $1.2 \times t_{UP} < t_{SCP}$.

There is a need to reduce C_{PC} or C_{SS} in order to achieve fast rise time. If the C_{SS} is decreased, the overshoot of the output voltage increases as the inrush current increases. On the other hand, if the C_{PC} is decreased, the phase margin becomes unstable due to the failure to start at the right timing when the recommended range of $1.2\times t_{UP} < t_{SCP}$ is not met. Also, always confirm that , CT terminal is connected to GND. The power supply voltage VCC after applying a PWM signal input, please input always earlier than the EN control signal when used in external input PWM as stated in P.19.

7. DC/DC controller

(1) Over-voltage protection circuit (OVP)

The output of the DCDC converter should be connected to the OVP pin via a voltage divider. In determining the appropriate trigger voltage of the OVP block, consider the total number of LEDs in series and the maximum V_F variation. The OVP terminal voltage, V_{OVP} is recommended to be in the range of 1.2V<V_{OVP}<1.4V during normal operation. If V_{OVP} is not at the normal operating range, it is possible to detect LED open protection. And the role of the OVP function is for the protection of the half-short mode of FB terminal short ($V_{FB} \approx 0.1 V$).

(2) DC/DC converter oscillation frequency (fosc)

The regulator's internal triangular wave oscillation frequency can be set via a resistor connected to the RT pin (pin 5). This resistor determines the charge/discharge current to the internal capacitor, thereby changing the oscillation frequency. Refer to the following theoretical formula when setting RT:

$$
f_{OSC} = \frac{60 \times 10^6}{R_{RT}[\Omega]} \times \alpha \, [kHz]
$$

60 x 10⁶ (V/A/S) is a constant (±5%) determined by the internal circuitry, and α is a correction factor that varies in relation to RT: (RT: α = 100kΩ: 1.0, 150kΩ: 0.99, 200kΩ: 0.98, 280kΩ: 0.97)

A resistor in the range of 100kΩ to 280kΩ is recommended. Settings that deviate from the frequency range shown below may cause switching to stop, causing the device operation to be unstable.

Please consider the parasitic capacitance of RT terminal at PCB board design. It must be less than 50pF.

(3) External DC/DC converter oscillation frequency synchronization (fSYNC)

Please do not switch from external to internal oscillation of the DC/DC converter if an external synchronization signal is present on the SYNC pin. When the signal on the SYNC terminal is switched from high to low, a delay of about 30 µs (typ) occurs before the internal oscillation circuit starts to operate (only the rising edge of the input clock signal on the SYNC terminal is recognized). Consider that; if the external sync is already running and is switched to internal synchronization from external synchronization. It may cause the output voltage overshoot and erroneous open detection may occur.

In addition, whenever an external synchronization is used, please set the R_{RT} such that the external synchronization frequency is $f_{\text{SYNC}} < f_{\text{OSC}} \times 1.2$.

(4) Soft Start Function

The soft-start (SS) limits the current and slows the rise-time of the output voltage during the start-up, and hence leads to the prevention of the overshoot of the output voltage and the inrush current. The SS voltage is Low when the OCP and the OVP is detected. Switching is stopped and operation is resumed.

 t_{SS} (soft-start time) is calculated using the formula below. Please refer to P.23 for more detailed application of the setting method.

Soft start time: t_{SS} Soft start charge current 5μA (Typ): Iss Capacitor of SS: Css Soft start release voltage 0.85V (Max): V_{SWST}

(5) Self-diagnostic functions

The operating status of the built-in protection circuit is propagated to FAIL1 and FAIL2 pins (open-drain outputs). FAIL1 becomes low when UVLO, TSD, OVP, OCP, or SCP protection is engaged, whereas FAIL2 becomes low when open or short LED is detected.

(6) Operation of the Protection Circuit

(a) Under-Voltage Lock Out (UVLO)

The UVLO shuts down all the circuits except for VREG when VCC $\leq 4.3V$ (TYP).

(b) Thermal Shut Down (TSD)

The TSD shuts down all the circuits except for REG when the Tj reaches 175°C (TYP), and releases when the Tj becomes below 150°C (TYP).

(c) Over Current Protection (OCP)

The OCP detects the current through the power-FET by monitoring the voltage of the high-side resistor and activates when the CS voltage becomes less than V_{CC} -0.6V (TYP). When the OCP is activated, the external capacitor of the SS pin will discharge and the switching operation of the DCDC turns off.

(d) Over Voltage Protection (OVP)

The output voltage of the DCDC is detected with the OVP-pin voltage and the protection activates when the OVP-pin voltage becomes greater than 2.0V (TYP). When the OVP is activated, the external capacitor of the SS pin will discharge and the switching operation of the DCDC turns off.

(7) Short Circuit Protection (SCP) (Following Figure 36 in P.21)

SCP is independent from PWM dimming. When the FB-pin voltage becomes less than 0.05V (TYP), the internal counter starts operating and latches off the circuit approximately after 150ms (when $C_{CT} = 0.1 \mu F$). If the FB-pin voltage becomes over 0.05V before 150ms, then the counter resets. When the LED anode (i.e. DCDC output voltage) is shorted to ground, the LED current turns off and the FB-pin voltage becomes low. Furthermore, the LED current also turns off when the LED cathode is shorted to ground. Hence in summary, the SCP works in both cases when the LED anode and the LED cathode is being shorted.

SCP mask timer (t_{SCP}) can be calculated using the following expression.

The need for SCP varies depending on the application. The OCP is detected and limited by High side SW, when the output is shorted to GND in the Buck / Buck-Boost application. Since the current continues to flow continuously, set the SCP timer to stop after an error is detected. On the other hand, the current path can not be cut off and large current continues to flow in the Boost application because there is no High side SW in Buck / Buck-Boost application. Therefore, please mask the SCP function in boost application. (CT terminal short to GND)

(8) LED Open Detection(Following Figure 34 in P.20)

When the FB-pin voltage $<$ 50mV (TYP) as well as OVP-pin voltage \geq 1.7V (TYP) operates in these ranges, the device detects LED open and latches off that particular channel.

(9) LED Short Detection(Following Figure 35 in P.20)

Less brightness of the light source will be produced whenever one LED is shorted somewhere within the load. If the guaranteed luminance of the light source is required, detection of the failure in the circuit must be performed. LED short detection is activated whenever one of the LEDs in the circuit, is shorted. In case of a short circuit, problem of LED short detection is informed. When one of the LEDs used is shorted somewhere in the circuit, [LEDR-LEDC| ≥ 0.2 (TYP), the internal counter starts operating, and approximately after 100ms (when $f_{\text{OSC}} = 300$ kHz) the operation latches off. With the PWM brightness control, the detection operation only proceeds when PWM=Hi. If the condition of the detection operation is released before 100ms (when $f_{\text{OSC}} = 300$ kHz), then the internal counter resets.

 $t_{SHORT} = 1/f_{OST} \times 32770 / DON$

 $\overline{\mathsf{LED}}$ short timer : t_{SHORT} DC/DC oscillator frequency: f_{OSC} PWM dimming ratio: DON

There is a possibility that the LED short detection malfunctions when the difference of V_F is large. Therefore, please adjust external resistance connected for V_F . It is recommended to be 1V-3V of the input voltage range of LEDR and LEDC.

(Note) The counter frequency is the DCDC switching frequency determined by the RT. The latch proceeds at the count of 32770.

Figure 27. High luminance LED (multichip) when using Y piece

Figure 28. When using the single chip (White LED) Figure 29. When using the Low V_F LED as Red LED

8. Error all condition

9. Effectiveness of the protection of each application

- Note1: When the DC/DC output is shorted to GND using Boost application, there is a possibility of high current flow which lead to the destruction of the external components. For the reduction of current in the external components, CT terminal is connected to GND.
- Note2:LED doesn't light when LED is shorted between anode and cathode. Under shorting LED, when using Buck/Buck-Boost application, may cause the large current not to flow while when using Boost application, there is a large current flowing from VCC to GND.

10. Power supply turning on sequence

Figure 33

Power supply turning on sequence

- ① After becoming V_{CC} >5V, the input of the other signals is possible.
② Before EN inputs, please fix VTH, THM, DRLIN, SYNC terminal v
- Before EN inputs, please fix VTH, THM, DRLIN, SYNC terminal voltage. An input order is not related.
- ③ VREG rises simultaneously with the input of EN, UVLO protection releases and switching starts.
- ④ VREG falls simultaneously with EN=Off.
- ⑤ Please stop input signal of VTH, THM, DRLIN, SYNC terminal voltage. An input order is not related.

⑥ VCC is OFF.

Note: It leads to the destruction of IC and external parts because it doesn't error output according to an external constant of adjacent pin 24pin SW terminal, 25pin OUTH terminal, 26pin CS terminal and 27pin BOOT terminal.

11. Operation in error circumstances of LED

(1) LED open detection

Figure 34

(2) LED short detection

It detects short and error is detected with FAIL2 after the timer TSHORT. Ex) TSHORT is about 100ms under the condition that FOSC=300kHz and dimming=100%. TSHORT is about 200ms under the condition that FOSC=300kHz and dimming=50%.

(3) LED anode short to GND detection

Figure 36

Note: When GND short-circuits by the DC/DC output by Boost application, high current flows and may lead to the destruction of external parts. The boost application does not enable the GND short protection of the DC/DC output.

12. Procedure for external components selection

(1) PWM dimming frequency and ratio setting

It is possible to set the PWM frequency (f_{PWM}) and the PWM on Duty (DON) in the external resistor and capacitor using the built-in CR timer function.

(2) SCP mask timer setting

SCP mask timer (t_{SCP}) is determined by the CT terminal capacitor which is calculated using the following expression.

 $\frac{\mu}{I_{CT}[\mu A]} \times 8$ count $t_{SCP} = \frac{C_{CT}[\mu F] \times V_{CT}[V]}{I}$ *CT* $SCP = \frac{C_{CT}[\mu r] \times V_{CT}[V]}{I_{CT}[\mu A]} \times 8$ $=\frac{C_{CT}[\mu F] \times V_{CT}[V]}{I_{CT}[\mu A]} \times$ μ

SCP mask timer: tscp CT charge current 5μA (Typ): Icτ Capacitor of $CT: C_{CT}$ CT terminal Voltage 0.8V (Typ): V_{CT}

In the P.14, when LED number is large or PWM dimming ratio is low, it may not satisfy the relational formula which has been described in P.14. Please connect CT terminal to GND in case the relational formula is not satisfied.

(3) Setting of the soft-start

The soft-start allows the coil current as well as the overshoot of the output voltage at the start-up to be minimized. For the capacitance, it is recommended to be in the range of $0.001\mu F \sim 0.1\mu F$. If the capacitance is less than $0.001\mu F$, it may cause an overshoot on the output voltage while if the capacitance is greater than 0.1µF, it may cause massive reverse current through the parasitic elements of the IC and may damage the whole device.

$$
t_{SS} = \frac{V_{SWST}[V] \times C_{SS}[\mu F]}{I_{SS}[\mu A]}
$$

(4) CPC setting that meets the condition of the rise time of the output voltage such that tUP < SCP mask timer tSCP The rise time of the output voltage (t_{UP}) can be calculated using the following formula.

 $t_{UP} = t_{SS} + t_{COMP}$

 $I_{COMPSOLRCE}[\mu A]$ *DON* $t_{COMP} = \frac{V_{SWMAX}[V] \times C_{PC}[\mu F]}{V_{VXX}}$ *COMPSOURCE* $\frac{V_{SWMAX}[V] \times C_{PC}[\mu] }{I} \times \frac{1}{P}$ $[\mu A]$ $=\frac{V_{SWMAX}[V]{\times}C_{PC}[\mu F]}{I_{COMPSOLRCE}[\mu A]} \times$ μ

Rise Time of the COMP voltage: t_{COMP} COMP source current: I_{COMPSOURCE} Capacitor of COMP: C_{PC} PWM Dimming rate: DON MaxDuty output voltage $2.0V$ (Max): V_{SWMAX}

Please adjust C_{PC} and C_{CT} to satisfy the following relationship.

 t_{UP} < t_{SCP}

For a guide, it is recommended that $1.2 \times t_{UP} < t_{SCP}$.

If the above formula is not satisfied, failure in the activation of the SCP may occur regardless of which application. So it is important to connect CT terminal to GND to prevent the false detection of SCP protection circuit.

(5) IL_MAX from the operating conditions.

(a) Calculation of the maximum output voltage (V_{OUT}) To calculate the V_{OUT} , it is necessary to take into account the V_F variation and the number of LEDs connected in series connection.

connection.
\n
$$
V_{OUT} = (V_F + \Delta V_F) \times N + V_{REF} + R_{PWMON} \times I_{OUT}
$$

(b) Calculation of the output current ILED

SET $LED = \frac{V_{REF}}{R_{SET}}$ $I_{LED} = \frac{V}{I}$

(c) Calculation of the input peak current I_{L} _{MAX}

Buck-Boost

$$
I_{L_MAX} = I_{L_AVG} + 1/2\Delta I_L
$$

\n
$$
I_{L_AVG} = (V_{CC} + V_{OUT}) \times I_{LED}/(\eta \times V_{CC})
$$

\n
$$
\Delta I_L = \frac{V_{CC}}{L} \times \frac{1}{f_{OSC}} \times \frac{V_{OUT}}{V_{CC} + V_{OUT}}
$$

Boost

$$
I_{L_MAX} = I_{L_AVG} + 1/2\Delta I_L
$$

\n
$$
I_{L_AVG} = V_{OUT} \times I_{LED}/(\eta \times V_{CC})
$$

\n
$$
\Delta I_L = \frac{V_{CC}}{L} \times \frac{V_{OUT} - V_{CC}}{V_{OUT}} \times \frac{1}{f_{OSC}}
$$

Buck

 $I_{L_MAX} = I_{L_MVG} + 1/2\Delta I_L$ I_L $_{AVG}$ = I_{LED} $L = \frac{V_{OUT}}{L} \times \frac{V_{CC} - V_{OUT}}{V_{OUT}} \times \frac{1}{f}$ $V_{CC} - V$ *L* $\Delta I_L = \frac{V_{OUT}}{V_{C}C} \times \frac{V_{CC} - V_{OUT}}{V_{C}C} \times \frac{1}{V_{C}C}$

- The worst case scenario for VCC is when it is at the minimum, and thus the minimum value should be applied in the equation.
- The L value of 6.8µH to 33µH is recommended. The current-mode type of DC/DC conversion is adopted for BD8381AEFV-M, which is optimized with the use of the recommended L value in the design stage. This recommendation is based upon the efficiency as well as the stability. The L values outside this recommended range may cause irregular switching waveform and hence deteriorate stable operation.
- η (Efficiency) is approximately 80% in Buck-Boost application and approximately 90% in Buck / Boost application.

(6) The setting of over-current protection

OUT JOSC

The setting of over-current protection
Choose R_{CS} µsing the formula $\frac{V_{OCP_MIN}}{V_{OCP_MIN}}(= 0.52 V) / R_{CS} > I_{L_MAX}$. When investigating the margin, please note that the L value may vary by approximately ±30%. And $I_{OCP_MAX} = V_{OCP_MAX}(0.68V) \div R_{CS}$.

 V_F of LED: V_F V_F distribution: ΔV_F Series of LED: N DC/DC feedback Ref voltage 0.2V (Typ): VREF ON Resistance of PWM dimming: R_{PWMON} LED current: I_{LED} PWM dimming ratio: DON Resistance of LED current setting: R_{SET} Coil max current: I_L _{MAX} Coil average current: I_L _{AVG} Ripple current:ΔI^L Power supply voltage: V_{cc} Output voltage: Vout Efficiency:η DC/DCFrequency: f_{OSC}

(7) The selection of the L

In order to achieve stable operation of the current-mode DC/DC converter, we recommend selecting the L value in the ranges indicated below:

$$
0.05\left[V/\mu s\right]<\frac{V_{OUT}\times R_{CS}}{L}<0.3\quad\left[V/\mu s\right]
$$

Boost

0.05
$$
[V/\mu s] < \frac{(V_{OUT} - V_{CC}) \times R_{CS}}{L} < 0.3
$$
 $[V/\mu s]$

Stability will be greatly increased by reducing the calculated value but there is also a possibility that the response will be lowered.

(8) The setting of OVP voltage

It is recommended that OVP terminal voltage is set from 1.2V to 1.4V. When V_{OVP} <1.2V, it is necessary that the external components are in high voltage ratings.. When $V_{OVP}>1.4V$, there is a possibility that LED open protection may malfunction and by determining R_{OVP1} and R_{OVP2} , V_{OUT_MAX} can be calculated using the following formula.

$$
V_{OUT_OVPMAX} = \frac{R_{OVPI} [k\Omega] + R_{OVP2} [k\Omega]}{R_{OVP2} [k\Omega]} \times V_{OVP}
$$

Output voltage at OVP detection: V_{OUT_OVPMAX} OVP resistance: R_{OVP1}, R_{OVP2} OVP detection voltage $2.1V$ (MAX): V_{OVP}

$$
1.2V < \frac{VOUT}{ROVP1 + ROVP2} \times ROVP < 1.4V
$$

Figure 37. The circuit of OVP terminal

(9) Select coil, schottky diodes, MOSFET and RCS which meet the ratings

(a) Buck-Boost application

Figure 38. Buck-Boost application

Note: In consideration of the external component variations, please design with sufficient margin.

Note: V_{CC_MAX} is the maximum supply voltage, V_{OUT_MAX} is the maximum output voltage detect by OVP.

(b) Boost application

Figure 39. Boost application

Note: In consideration of the external component variations, please design with sufficient margin.

Note: V_{CC_MAX} is the maximum supply voltage, V_{OUT_MAX} is the maximum output voltage detect by OVP.

(c) Buck application

Note: In consideration of the external component variations, please design with sufficient margin. Note: V_{CC_MAX} is the maximum supply voltage, V_{OUT_MAX} is the maximum output voltage detect by OVP.

(10) Selection of the output capacitor

Select the output capacitor C_{OUT} based on the requirement of the ripple voltage Vpp.

Buck-Boost

$$
Vpp = \frac{I_{LED}}{C_{OUT}} \times \frac{V_{CC}}{V_{OUT} + V_{CC}} \times \frac{1}{f_{OSC}} + (I_{L_MAX + \Delta I_L/2}) \times R_{ESR}
$$

ESR of output capacitor : RESR

Buck

$$
Vpp = \frac{1}{C_{OUT}} \times \frac{I_{LED}}{\eta} \times \frac{1}{f_{OSC}} + (I_{L_MAX} \times R_{ESR})
$$

Ī. **Boost**

$$
Vpp = \Delta I_L \times R_{ESR} + \frac{\Delta I_L}{8} \times \frac{1}{C_{OUT}} \times \frac{1}{f_{OSC}}
$$

(11) Selection of the input capacitor

A capacitor at the input is also required as the peak current flows between the input and the output terminals in DC/DC conversion. We recommend an input capacitor greater than 10µF with the ESR smaller than 100mΩ. The input capacitor outside of our recommendation may cause large ripple voltage at the input and hence may lead to malfunction.

(12) Phase Compensation Guidelines

In general, the negative feedback loop is stable when the following condition is met:

- (a) Overall gain of 1 (0dB) with a phase lag of less than 150º (i.e., Phase margin of 30º or more) However, as the DC/DC converter constantly samples the switching frequency, the gain-bandwidth (GBW) product of the entire series should be set to 1/10 of the switching frequency of the system. Therefore, the overall stability characteristics of the application are as follows:
- (b) Overall gain of 1 (0dB) with a phase lag of less than 150º (i.e., Phase margin of 30º or more)
- (c) GBW (frequency at gain 0dB) of 1/10 of the switching frequency
	- Thus, to improve response within the GBW product limits, the switching frequency must be increased.

The key for achieving stability is to place fz near to the GBW. GBW is decided by phase delay fp1 in terms of C_{OUT} and output impedance R_L . fz and fp1 are defined by the following formula.

Good stability would be obtained when the fz is set between 1kHz to 10kHz. Please substitute the value of the maximum load for RL.

In Buck-Boost/ Buck application, Right-Hand-Plane (RHP) Zero exists. This Zero has no gain but a pole characteristic in terms of phase. As this Zero would cause instability when it is in the control loop, it is necessary to bring this zero before the GBW.

$$
f_{RHP} = \frac{V_{OUT} \times (V_{CC}/(V_{OUT} + V_{CC}))^2}{2\pi \times I_{OUT} \times L} \quad [Hz]
$$

where: *IOUT*: Maximum Load Current

It is important to keep in mind that these are very loose guidelines, and adjustments may have to be made to ensure stability in the actual circuit. It is also important to note that stability characteristics can change greatly depending on factors such as substrate layout and load conditions. Therefore, when designing for mass-production, stability should be thoroughly investigated and confirmed in the actual physical design.

(13) Verification of the operation by taking measurements

The overall characteristic may change by load current, input voltage, output voltage, inductance, load capacitance, switching frequency and the PCB layout. We strongly recommend verifying your design by taking the actual measurements.

13. Calculation of the Power consumption

Ciss1:External FET capacity of DC/DC switching

f_{OSC}: DC/DC switching frequency

- C_{iss2} : External FET capacity of PWM dimming
- *f*_{*PWM*}: PWM frequency

N: PCB layers

<Sample Calculation > When we assume value for Pc such as:

 $\rm\,I_{CC}$ =7mA, $\rm\,V_{CC}$ =30V, $\rm\,C_{iss1}$ =500pF, $\rm\,f_{\rm \,SSC}$ =300kHz, $\rm\,f_{\rm \,FWM}$ =200Hz, $\rm\,C_{iss2}$ =1500pF, N=4Layer

$$
\epsilon
$$
Sample Calculation > When we assume value for Pc such as:
cc=7mA, V_{CC}=30V, C_{iss1}=500pF, f_{osc}=300kHz, f_{PWM}=200Hz, C_{iss2}=1500pF, N=4Layer

$$
Pc(4) = 7mA \times 30V + \frac{1}{2} \times 500 pF \times 5V \times 300 kHz \times 5V \times 2 \times 2 + \frac{1}{2} \times 1500 pF \times 5V \times 200 Hz \times 5V \times 2
$$

it becomes Pc = approximately 210mW.

Figure 41

Note1: The value of Power consumption: on glass epoxy board measuring 70mmx70mmx1.6mm (1 layer board/Copper foil thickness 18um)

Note2: The value changes depending on the density of the board copper foil.

 However, this value is an actual measurement value and no guarantee value. HTSSOP-B28

- Pd=1.85W (0.37W): Board copper foil area 225mm²
- Pd=3.30W (0.66W): Board copper foil area 4900mm²

Pd=4.70W $(0.94W)$: Board copper foil area 4900mm²

The value in () is an power dissipation in Ta = 125 degrees.

I/O Equivalent Circuits

(Note) The values are all Typ value.

I/O Equivalent Circuits – continued

(Note) The values are all Typ value.

Operational Notes

1. **Reverse Connection of Power Supply**

Connecting the power supply in reverse polarity can damage the IC. Take precautions against reverse polarity when connecting the power supply, such as mounting an external diode between the power supply and the IC's power supply pins.

2. **Power Supply Lines**

Design the PCB layout pattern to provide low impedance supply lines. Separate the ground and supply lines of the digital and analog blocks to prevent noise in the ground and supply lines of the digital block from affecting the analog block. Furthermore, connect a capacitor to ground at all power supply pins. Consider the effect of temperature and aging on the capacitance value when using electrolytic capacitors.

3. **Ground Voltage**

Ensure that no pins are at a voltage below that of the ground pin at any time, even during transient condition.

4. **Ground Wiring Pattern**

When using both small-signal and large-current ground traces, the two ground traces should be routed separately but connected to a single ground at the reference point of the application board to avoid fluctuations in the small-signal ground caused by large currents. Also ensure that the ground traces of external components do not cause variations on the ground voltage. The ground lines must be as short and thick as possible to reduce line impedance.

5. **Thermal Consideration**

Should by any chance the power dissipation rating be exceeded the rise in temperature of the chip may result in deterioration of the properties of the chip. In case of exceeding this absolute maximum rating, increase the board size and copper area to prevent exceeding the Pd rating.

6. **Recommended Operating Conditions**

These conditions represent a range within which the expected characteristics of the IC can be approximately obtained. The electrical characteristics are guaranteed under the conditions of each parameter.

7. **Inrush Current**

When power is first supplied to the IC, it is possible that the internal logic may be unstable and inrush current may flow instantaneously due to the internal powering sequence and delays, especially if the IC has more than one power supply. Therefore, give special consideration to power coupling capacitance, power wiring, width of ground wiring, and routing of connections.

8. **Operation Under Strong Electromagnetic Field**

Operating the IC in the presence of a strong electromagnetic field may cause the IC to malfunction.

9. **Testing on Application Boards**

When testing the IC on an application board, connecting a capacitor directly to a low-impedance output pin may subject the IC to stress. Always discharge capacitors completely after each process or step. The IC's power supply should always be turned off completely before connecting or removing it from the test setup during the inspection process. To prevent damage from static discharge, ground the IC during assembly and use similar precautions during transport and storage.

10. **Inter-pin Short and Mounting Errors**

Ensure that the direction and position are correct when mounting the IC on the PCB. Incorrect mounting may result in damaging the IC. Avoid nearby pins being shorted to each other especially to ground, power supply and output pin. Inter-pin shorts could be due to many reasons such as metal particles, water droplets (in very humid environment) and unintentional solder bridge deposited in between pins during assembly to name a few.

Operational Notes – continued

11. **Unused Input Pins**

Input pins of an IC are often connected to the gate of a MOS transistor. The gate has extremely high impedance and extremely low capacitance. If left unconnected, the electric field from the outside can easily charge it. The small charge acquired in this way is enough to produce a significant effect on the conduction through the transistor and cause unexpected operation of the IC. So unless otherwise specified, unused input pins should be connected to the power supply or ground line.

12. **Regarding the Input Pin of the IC**

This monolithic IC contains P+ isolation and P substrate layers between adjacent elements in order to keep them isolated. P-N junctions are formed at the intersection of the P layers with the N layers of other elements, creating a parasitic diode or transistor. For example (refer to figure below):

When GND > Pin A and GND > Pin B, the P-N junction operates as a parasitic diode. When GND > Pin B, the P-N junction operates as a parasitic transistor.

Parasitic diodes inevitably occur in the structure of the IC. The operation of parasitic diodes can result in mutual interference among circuits, operational faults, or physical damage. Therefore, conditions that cause these diodes to operate, such as applying a voltage lower than the GND voltage to an input pin (and thus to the P substrate) should be avoided.

Figure 42. Example of monolithic IC structure

13. **Area of Safe Operation (ASO)**

Operate the IC such that the output voltage, output current, and power dissipation are all within the Area of Safe Operation (ASO).

14. **Thermal Shutdown Circuit(TSD)**

This IC has a built-in thermal shutdown circuit that prevents heat damage to the IC. Normal operation should always be within the IC's power dissipation rating. If however the rating is exceeded for a continued period, the junction temperature (Tj) will rise which will activate the TSD circuit that will turn OFF all output pins. When the Tj falls below the TSD threshold, the circuits are automatically restored to normal operation.

Note that the TSD circuit operates in a situation that exceeds the absolute maximum ratings and therefore, under no circumstances, should the TSD circuit be used in a set design or for any purpose other than protecting the IC from heat damage.

Ordering Information

Marking Diagram

Physical Dimension, Tape and Reel Information

Revision History

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	- [h] Use of the Products in places subject to dew condensation
- 4. The Products are not subject to radiation-proof design.
- 5. Please verify and confirm characteristics of the final or mounted products in using the Products.
- 6. In particular, if a transient load (a large amount of load applied in a short period of time, such as pulse. is applied, confirmation of performance characteristics after on-board mounting is strongly recommended. Avoid applying power exceeding normal rated power; exceeding the power rating under steady-state loading condition may negatively affect product performance and reliability.
- 7. De-rate Power Dissipation (Pd) depending on Ambient temperature (Ta). When used in sealed area, confirm the actual ambient temperature.
- 8. Confirm that operation temperature is within the specified range described in the product specification.
- 9. ROHM shall not be in any way responsible or liable for failure induced under deviant condition from what is defined in this document.

Precaution for Mounting / Circuit board design

- 1. When a highly active halogenous (chlorine, bromine, etc.) flux is used, the residue of flux may negatively affect product performance and reliability.
- 2. In principle, the reflow soldering method must be used on a surface-mount products, the flow soldering method must be used on a through hole mount products. If the flow soldering method is preferred on a surface-mount products, please consult with the ROHM representative in advance.

For details, please refer to ROHM Mounting specification

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	- [b] the temperature or humidity exceeds those recommended by ROHM
	- [c] the Products are exposed to direct sunshine or condensation
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- 3. Store / transport cartons in the correct direction, which is indicated on a carton with a symbol. Otherwise bent leads may occur due to excessive stress applied when dropping of a carton.
- 4. Use Products within the specified time after opening a humidity barrier bag. Baking is required before using Products of which storage time is exceeding the recommended storage time period.

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